

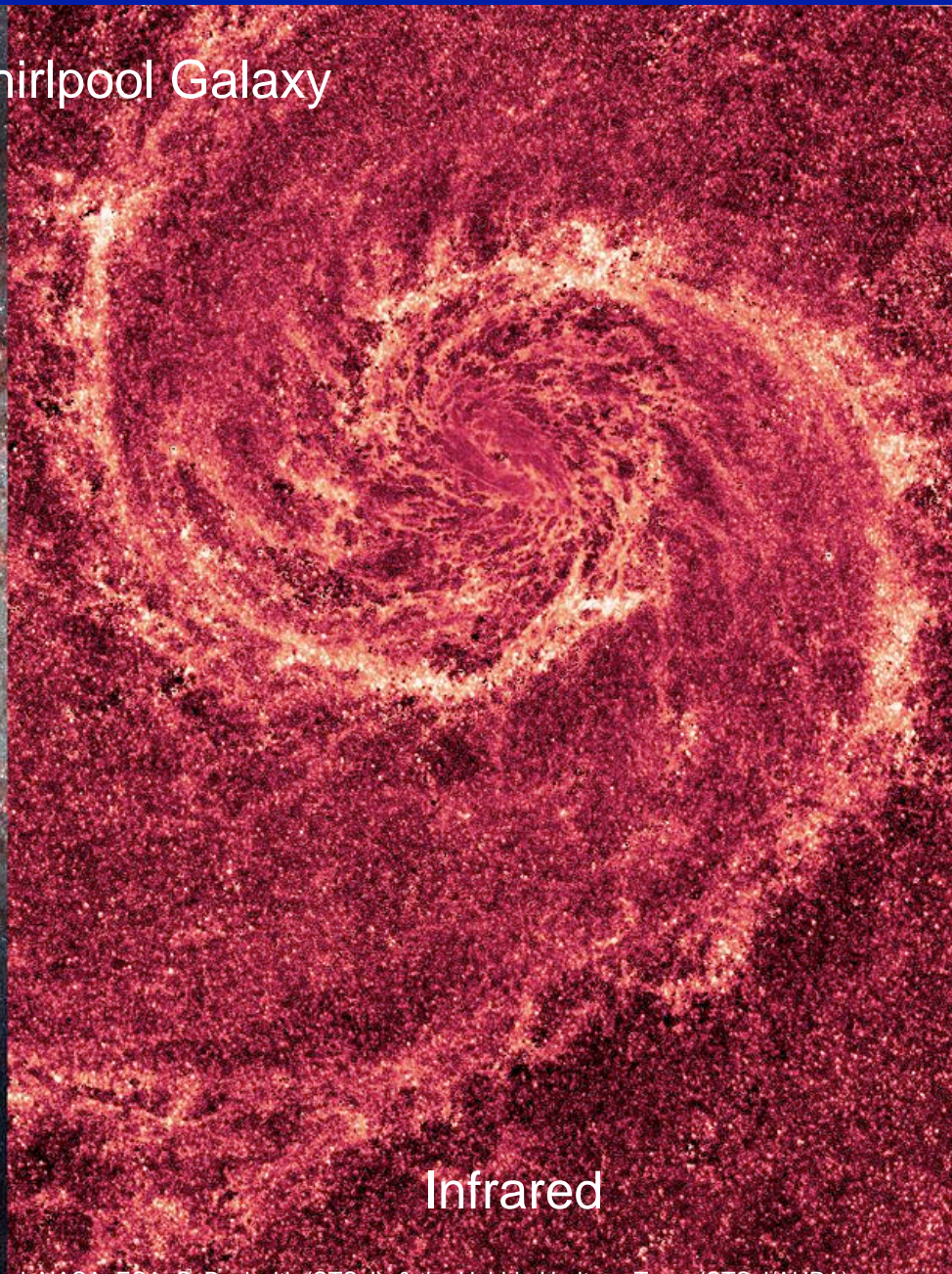
Grid-based Hydrodynamics

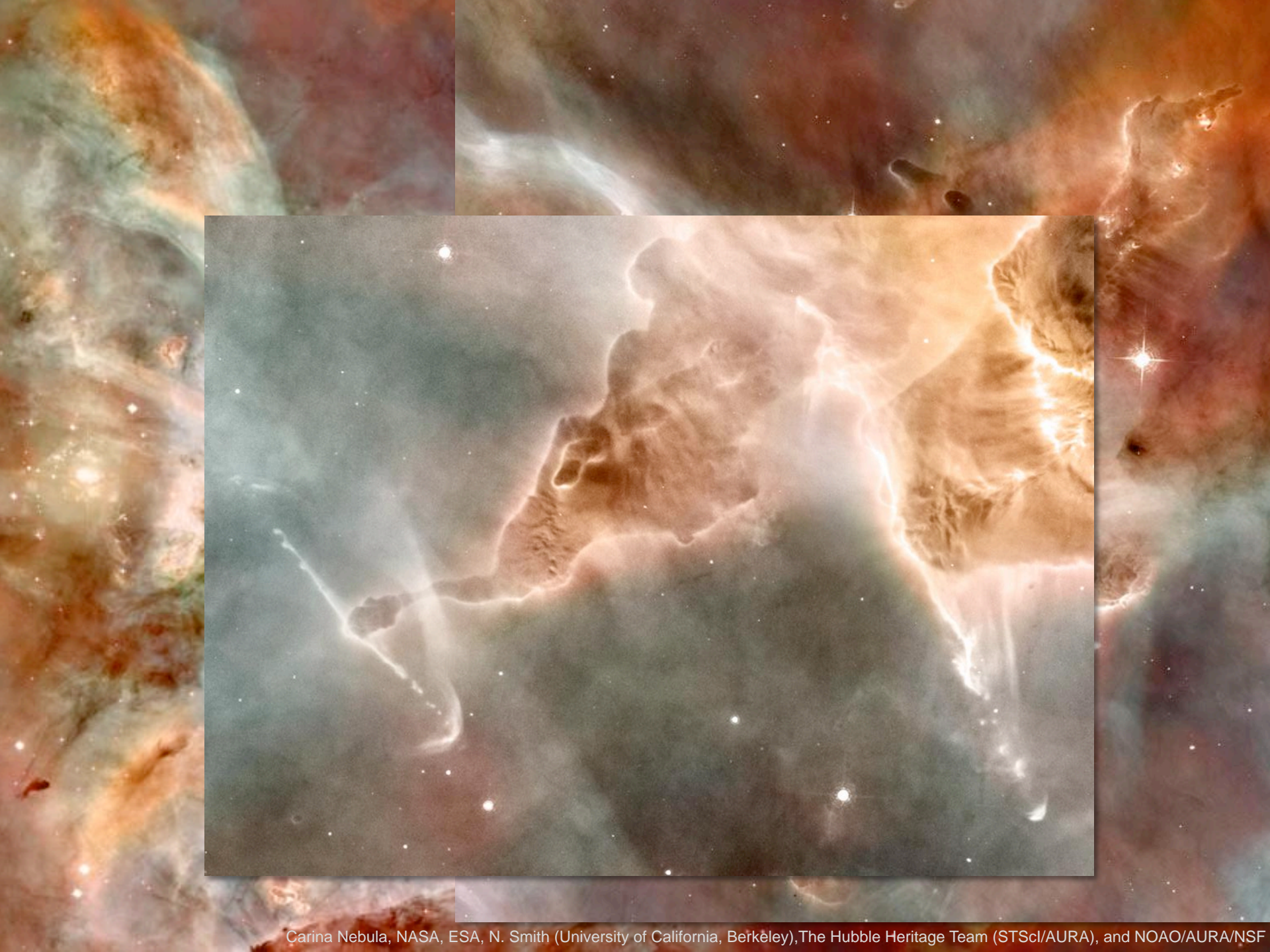
Christoph Federrath

- Complex fluid dynamics (equations are non-linear, 3D)
- Complex physics: turbulence, gravity, radiation, magnetic fields, etc.
- Large spatial and temporal scales involved

Star Formation

M51: The Whirlpool Galaxy

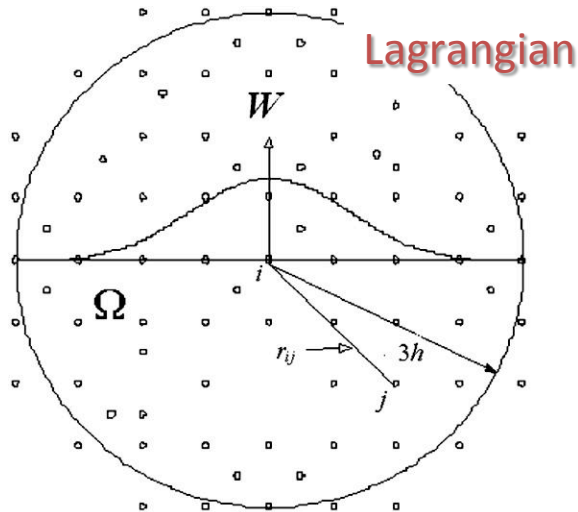




Carina Nebula, NASA, ESA, N. Smith (University of California, Berkeley), The Hubble Heritage Team (STScI/AURA), and NOAO/AURA/NSF

Fundamentals of SPH and grid

Smoothed Particle Hydrodynamics (SPH)
(Lucy 1977; Gingold & Monaghan 1977)

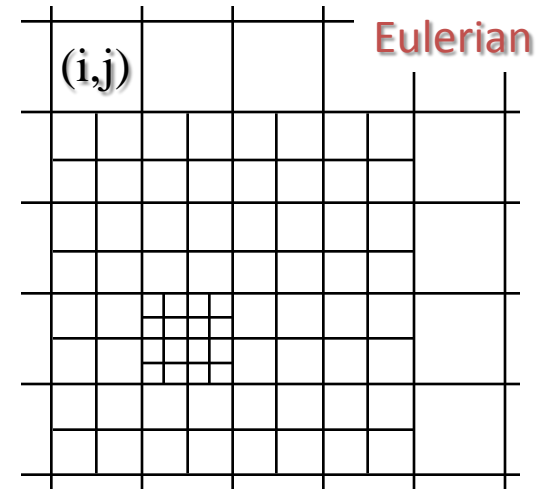


$$\rho(\mathbf{r}) = \sum_b m_b W(\mathbf{r} - \mathbf{r}_b, h)$$

$$\nabla A(\mathbf{r}) = \sum_b m_b \frac{A_b}{\rho_b} \nabla W(\mathbf{r} - \mathbf{r}_b, h)$$

$$W(x, h) = \frac{1}{h\sqrt{\pi}} e^{-(x^2/h^2)}$$

Adaptive Mesh Refinement (AMR)
(Berger & Collela 1989)

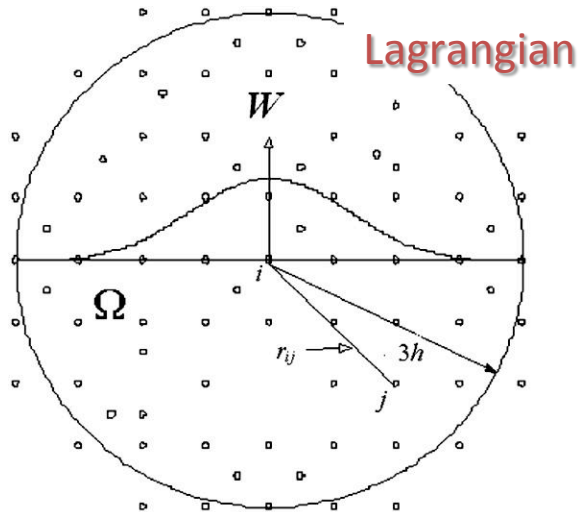


- Hydro variables are averages in cells
- Compute fluxes through cell faces
- Simple data structure: indexing
- Finite Volume vs. Finite Difference

R. Leveque: „Nonlinear Conservation Laws and Finite Volume Methods for Astrophysical Fluid Flow“

Fundamentals of SPH and grid

Smoothed Particle Hydrodynamics (SPH)
(Lucy 1977; Gingold & Monaghan 1977)

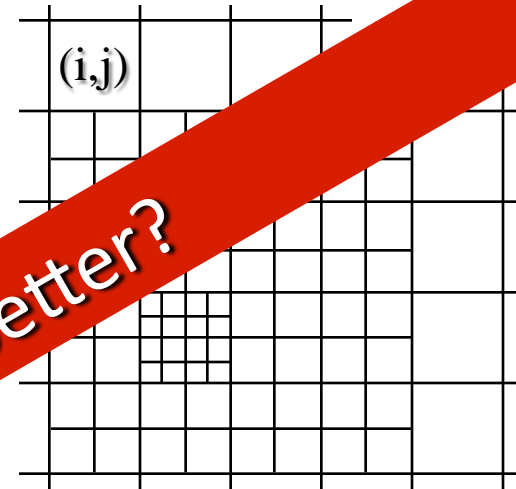


$$\rho(\mathbf{r}) = \sum_b m_b W(\mathbf{r} - \mathbf{r}_b, h)$$

$$\nabla A(\mathbf{r}) = \sum_b m_b \nabla W(\mathbf{r} - \mathbf{r}_b, h)$$

$$W(x, h) = \frac{1}{h\sqrt{\pi}} e^{-(x^2/h^2)}$$

Adaptive Mesh Refinement (AMR)
(Berger & Collela 1989)



Which method is better?

- Hydro variables are averages in cells
- Compute fluxes through cell faces
- Simple data structure: indexing
- Finite Volume vs. Finite Difference

R. Leveque: „Nonlinear Conservation Laws and Finite Volume Methods for Astrophysical Fluid Flow“

Comparison of SPH and grid in supersonic turbulence

TWO REGIMES OF TURBULENT FRAGMENTATION AND THE STELLAR INITIAL MASS FUNCTION FROM PRIMORDIAL TO PRESENT-DAY STAR FORMATION

PAOLO PADOAN,¹ ÅKE NORDLUND,² ALEXEI G. KRITSUK,¹ MICHAEL L. NORMAN,¹ AND PAK SHING LI³

Received 2006 October 16; accepted 2007 February 16

Their conclusion:

“ SPH simulations of large scale star formation to date fail in all three fronts: numerical diffusivity, numerical resolution, and presence of magnetic fields. This should cast serious doubts on the value of comparing predictions based on SPH simulations with observational data (see also Agertz et al. 2006). “

Driven turbulence comparison of SPH and grid

Motivation (role of supersonic turbulence for star formation)

Setup (Phantom and FLASH):

1. Same initial conditions: uniform density, zero velocities
2. Same turbulence forcing!
3. Driven to Mach number 10
4. Resolutions: 128^3 , 256^3 and 512^3 (**134,217,728**) both grid and SPH

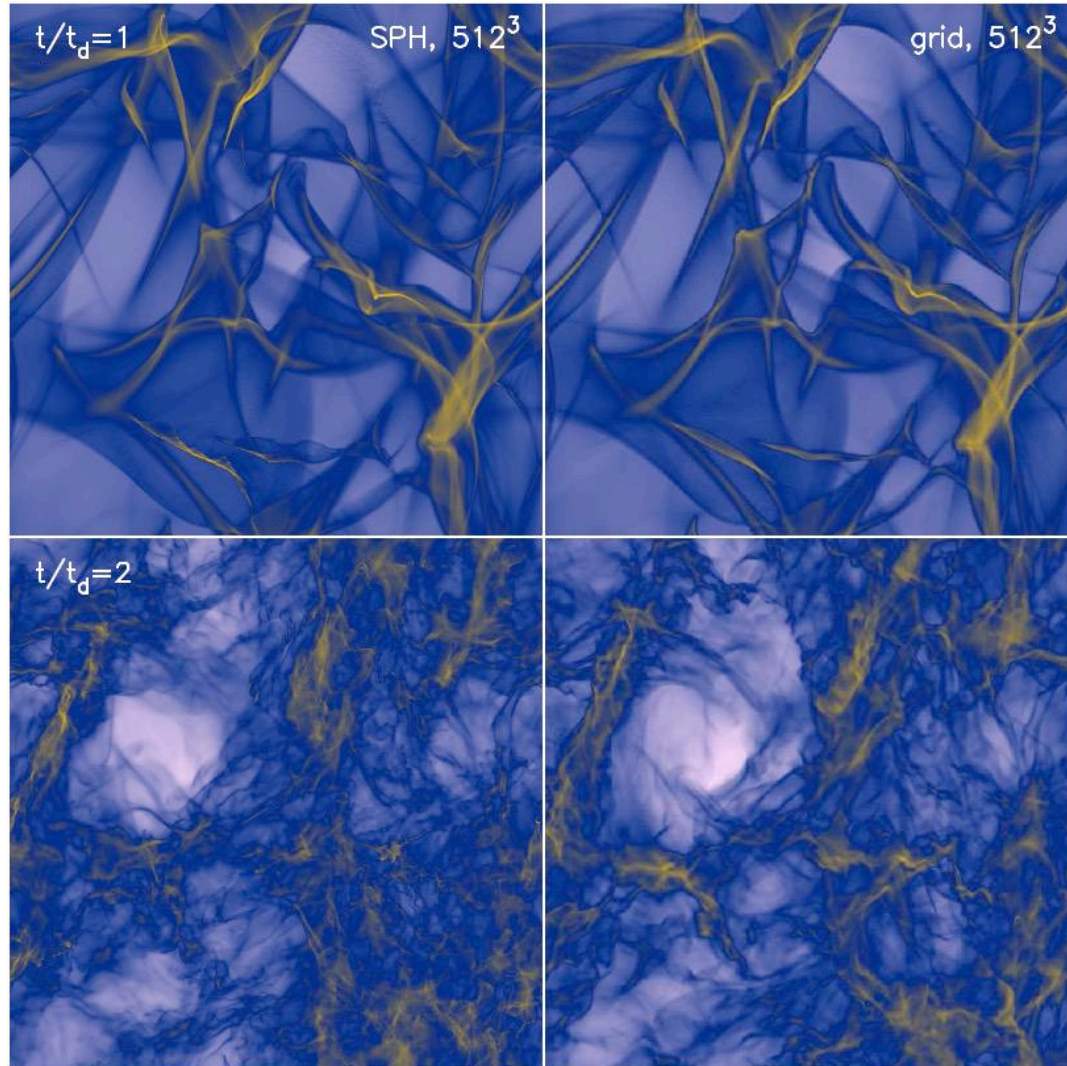
(Price & Federrath 2010, MNRAS 406, 1659)

Driven turbulence comparison of SPH and grid

Phantom

Column density

FLASH

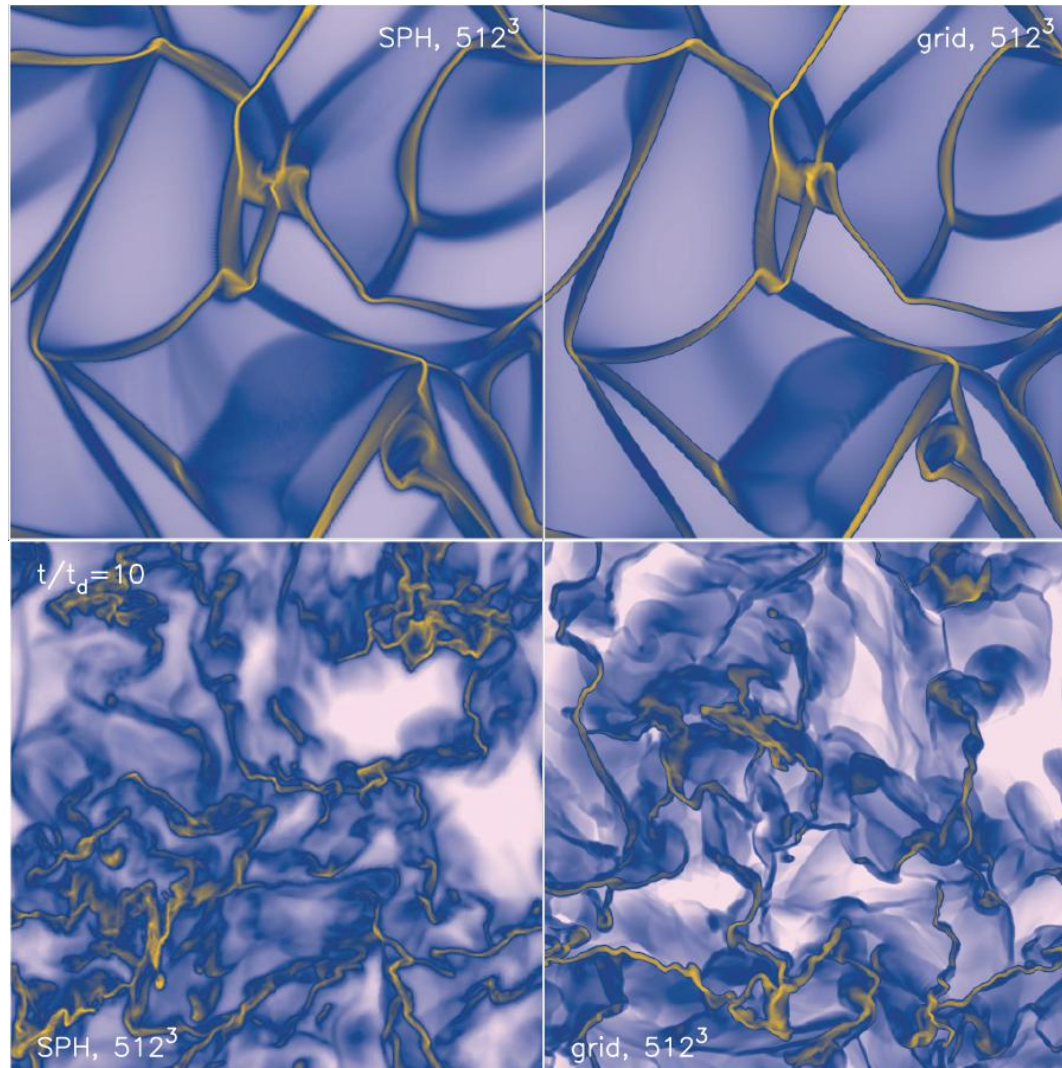


Driven turbulence comparison of SPH and grid

Phantom

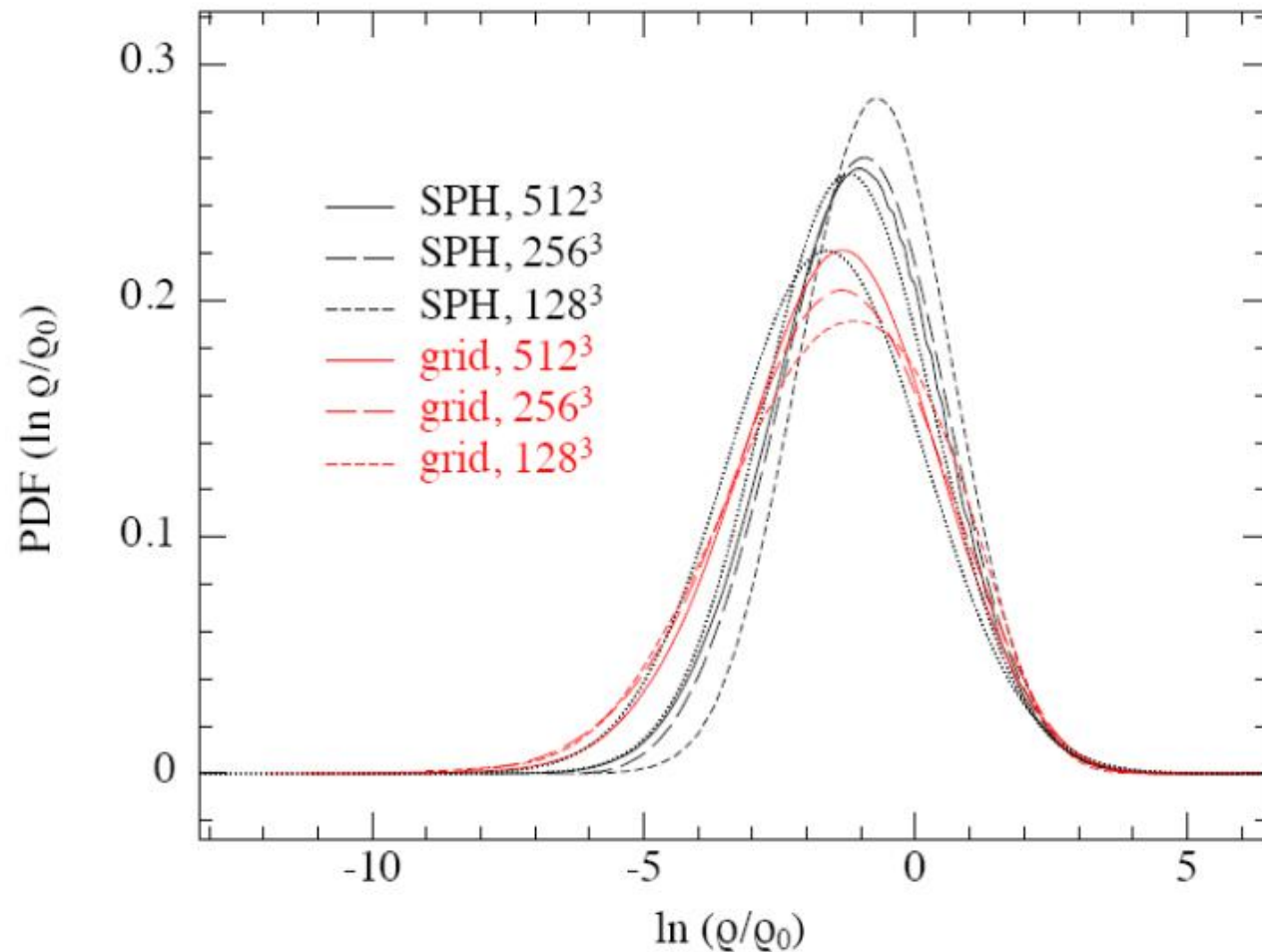
Slices of density

FLASH



Driven turbulence comparison of SPH and grid

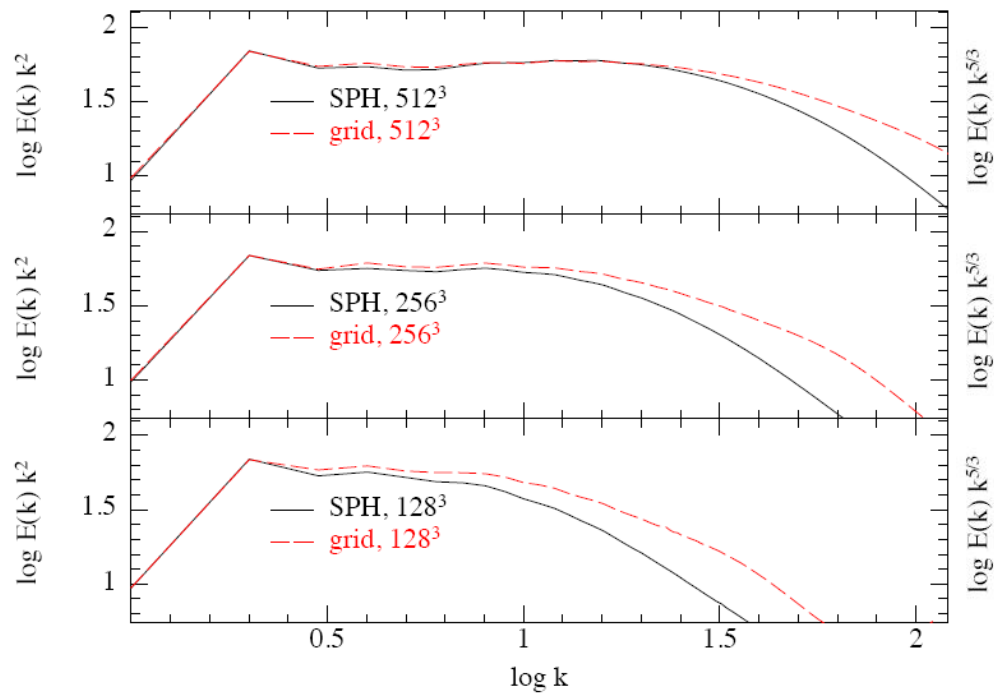
Density Probability Distribution Function (PDF):



PDFs converge with higher resolution

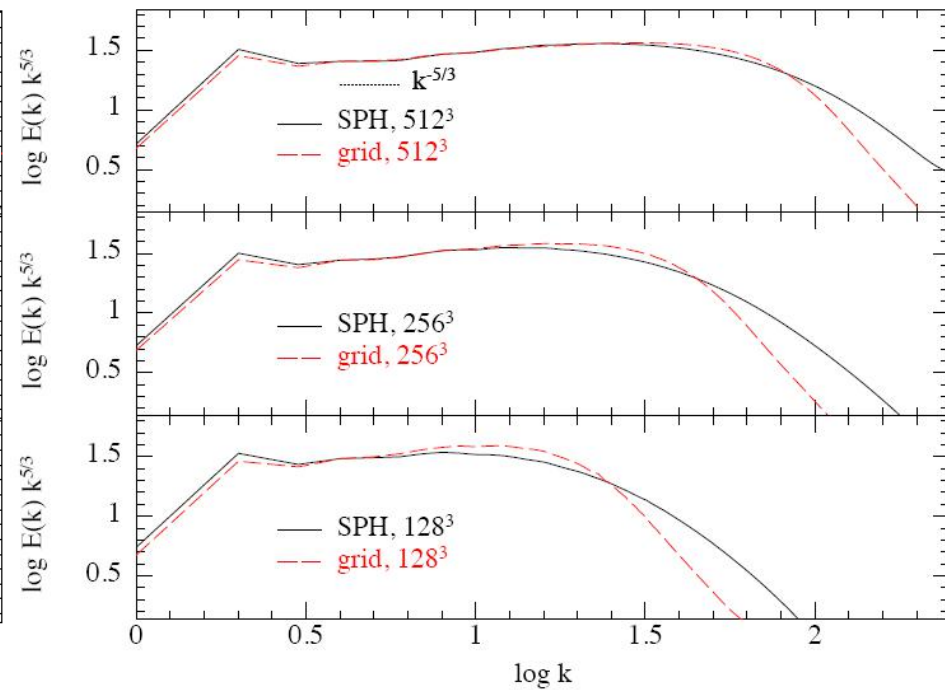
Driven turbulence comparison of SPH and grid

Velocity spectra, v (VOLUME-weighted)



Grid code less dissipative

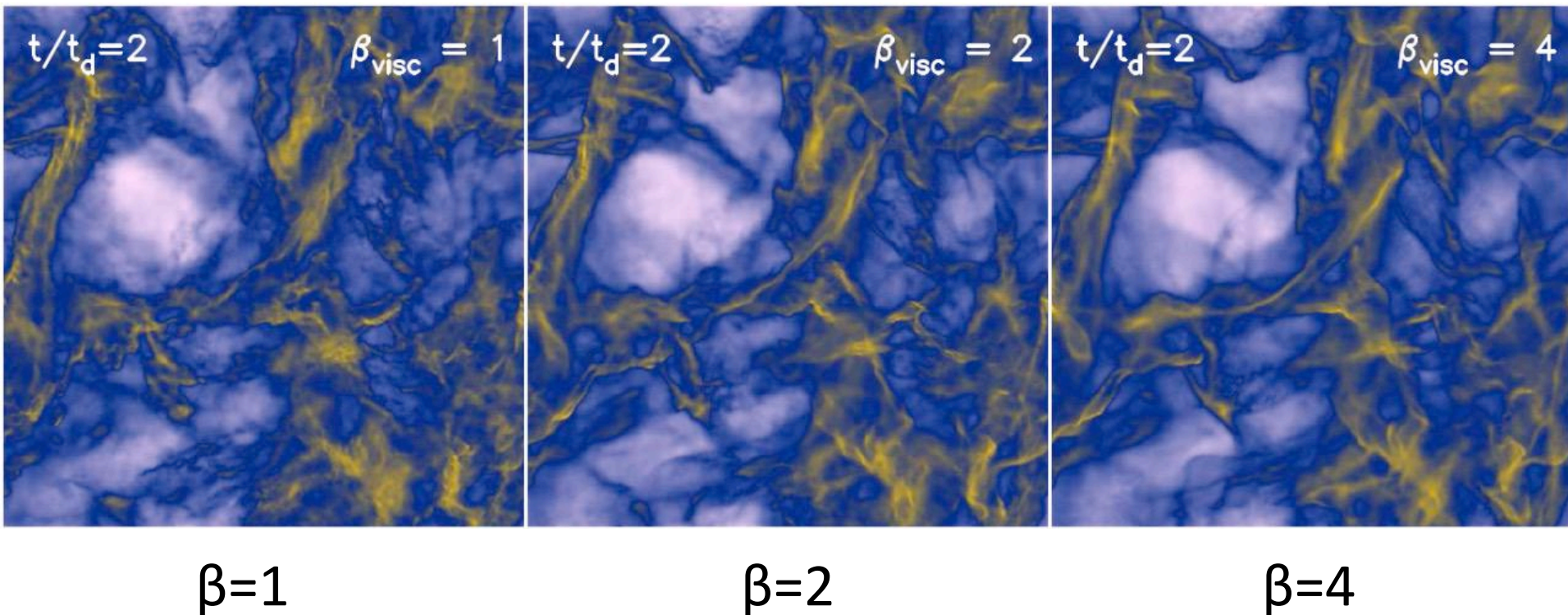
Velocity spectra, $\rho^{1/3}v$ (DENSITY-weighted)



SPH code slightly less dissipative

Driven turbulence comparison of SPH and grid

Influence of β -viscosity in SPH on the modelling of strong shocks



Particle interpenetration for $\beta < 4$

Driven turbulence comparison of SPH and grid

Conclusion

(Price & Federrath 2010, MNRAS 406, 1659)

Convergence of SPH and grid

Computational time pure hydro (**no gravity**):

FLASH grid about 20 times faster than Phantom SPH

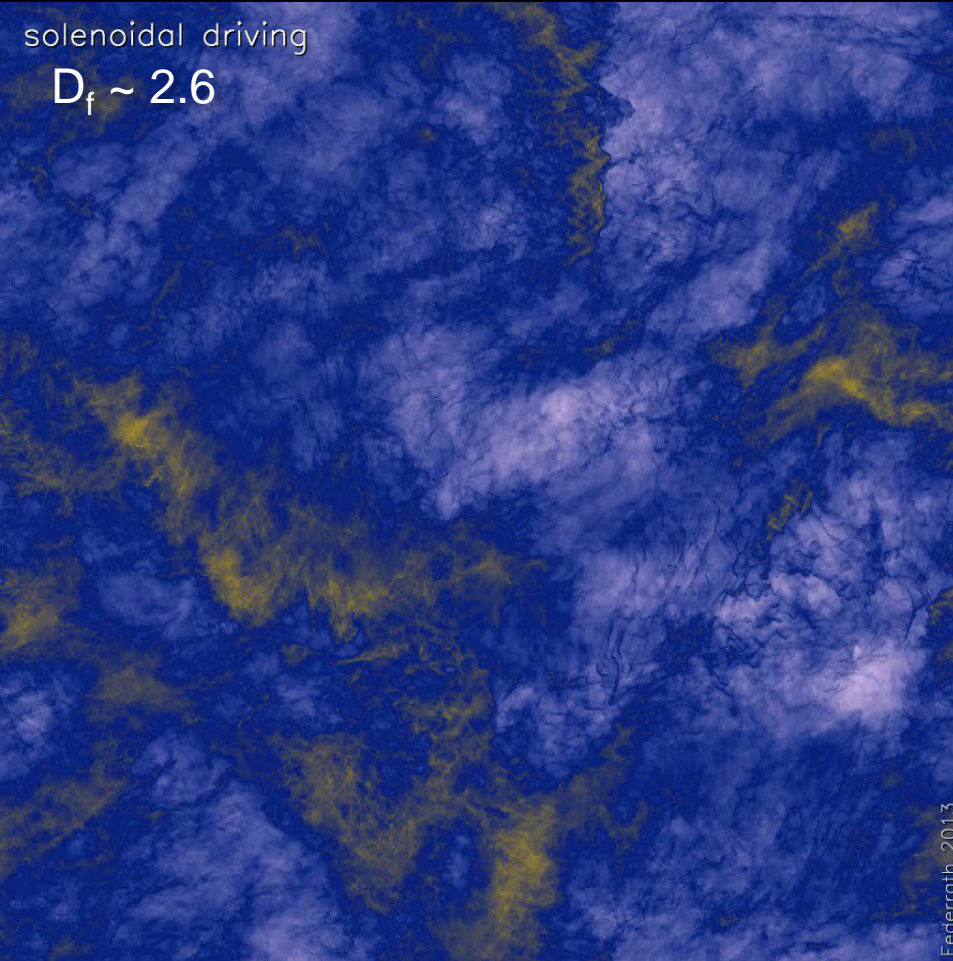
Hydrodynamical Turbulence

Movies available: <http://www.mso.anu.edu.au/~chfeder/pubs/supersonic/supersonic.html>

World's largest simulations of turbulence using **4096³ grid cells**

solenoidal driving

$D_f \sim 2.6$

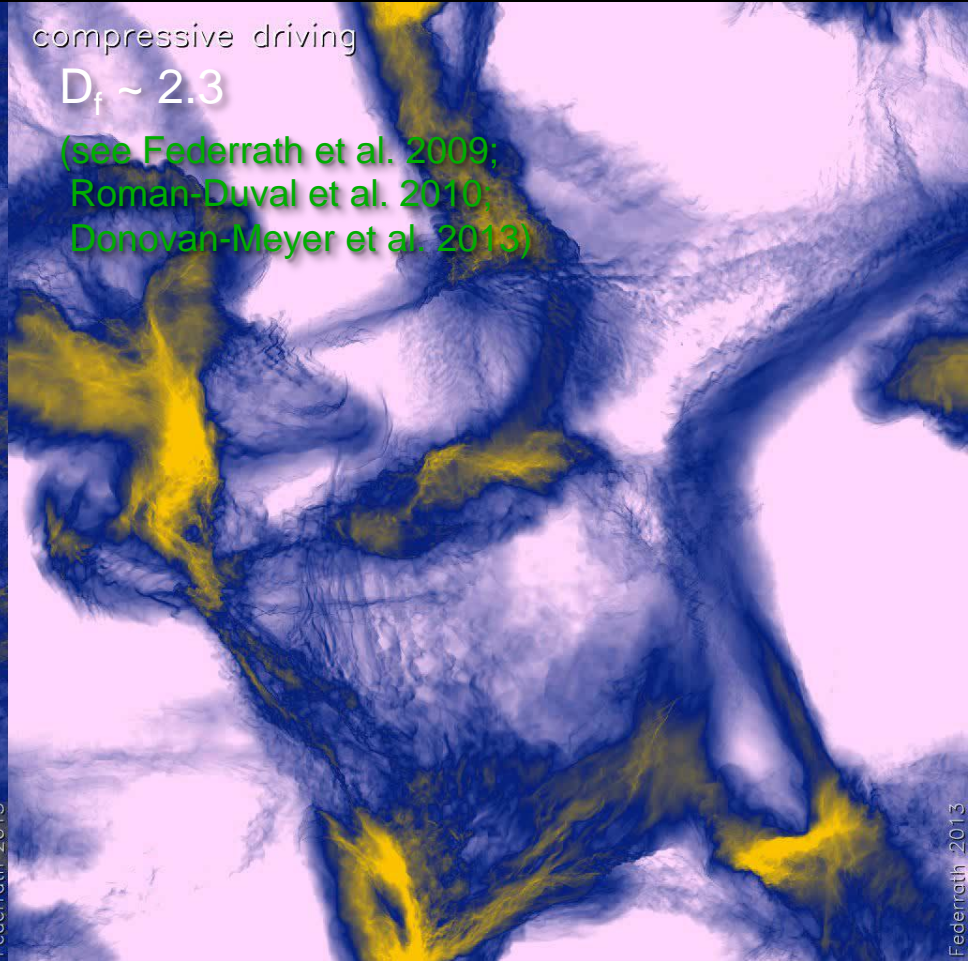


Federrath 2013

compressive driving

$D_f \sim 2.3$

(see Federrath et al. 2009;
Roman-Duval et al. 2010;
Donovan-Meyer et al. 2013)



Federrath 2013

(Federrath 2013, MNRAS 436, 1245: Supersonic turbulence @ 4096³ grid cells)

The basics of grid-based hydrodynamics

1. Introduction
2. Equations of hydrodynamics
3. Advection
4. Flux conservation and flux limiters
5. Conservative grid-based hydrodynamics
6. Basics of Riemann problem -> Riemann solvers
7. Adaptive-mesh refinement and sink particles

Lecture based on a lecture given by Kees Dullemond, 2009/2010, Heidelberg

Literature: Randall J. LeVeque, "Finite Volume Methods for Hyperbolic Problems"
(Cambridge Texts in Applied Mathematics)

The basics of grid-based hydrodynamics

Advection test, IDL code

Flux-conserving grid-based hydrodynamics

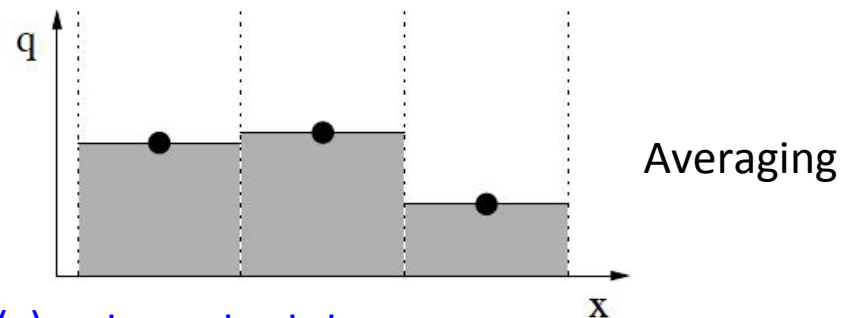
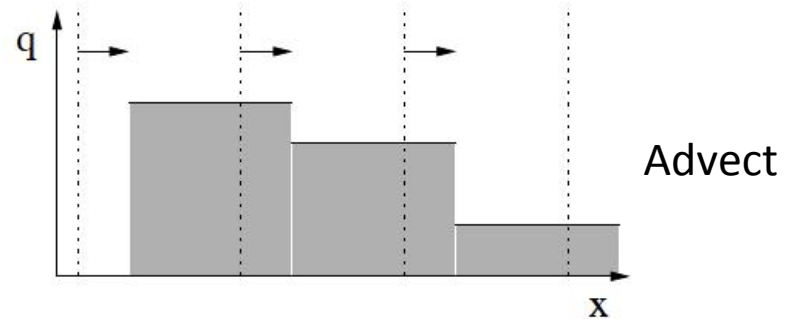
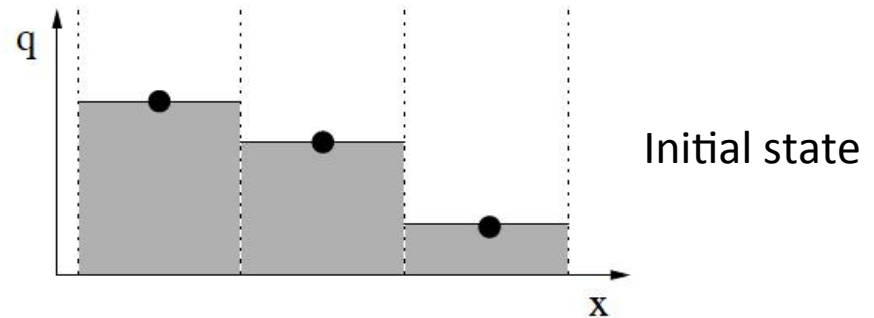
Donor-cell advection:

Piecewise constant subgrid model:

$$\tilde{q}_{i+1/2}^{n+1/2} = \begin{cases} q_i^n & \text{for } u_{i+1/2} > 0 \\ q_{i+1}^n & \text{for } u_{i+1/2} < 0 \end{cases}$$

Flux:

$$f_{i+1/2}^{n+1/2} = \begin{cases} u_{i+1/2} q_i^n & \text{for } u_{i+1/2} > 0 \\ u_{i+1/2} q_{i+1}^n & \text{for } u_{i+1/2} < 0 \end{cases}$$



Like upwind scheme, but works for $u(x)$ not constant, too.

Flux-conserving grid-based hydrodynamics

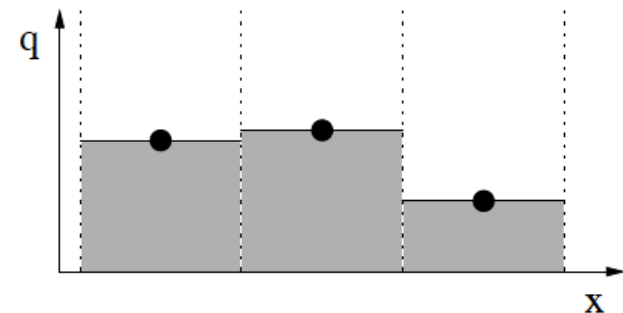
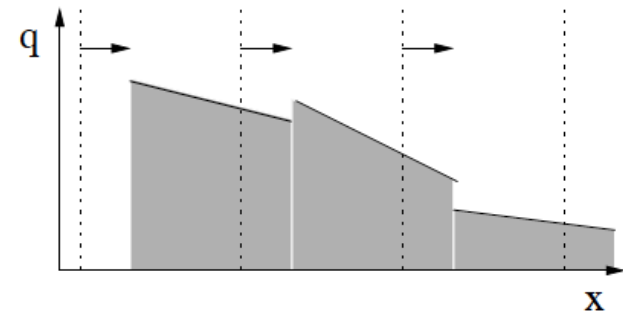
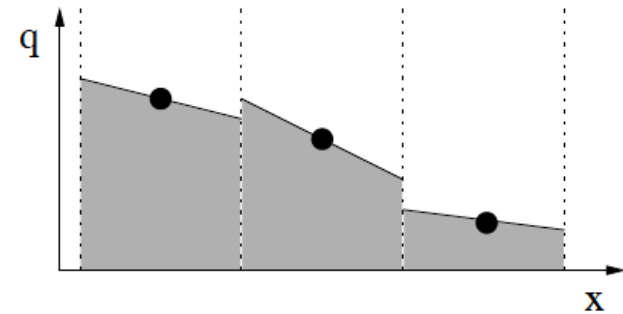
Piecewise linear subgrid model for flux:

- Donor-cell is quite diffusive ->
Use higher-order subgrid model

$$q(x, t = t_n) = q_i^n + \sigma_i^n (x - x_i)$$

↑
(slope)

Choice of slope



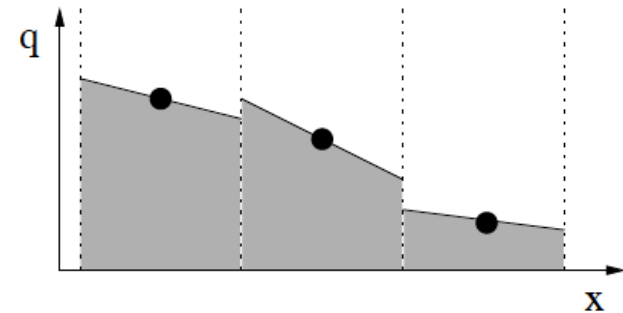
„MUSCL (Monotonic Upwind-centered Scheme for Conservation Laws)“

Flux-conserving grid-based hydrodynamics

Piecewise linear subgrid model for flux:

- Donor-cell is quite diffusive ->
Use higher-order subgrid model

$$q(x, t = t_n) = q_i^n + \sigma_i^n (x - x_i)$$



Different slope choices:

Centered slope: $\sigma_i^n = \frac{q_{i+1}^n - q_{i-1}^n}{2\Delta x}$ (Fromm's method)

Upwind slope: $\sigma_i^n = \frac{q_i^n - q_{i-1}^n}{\Delta x}$ (Beam-Warming method)

Downwind slope: $\sigma_i^n = \frac{q_{i+1}^n - q_i^n}{\Delta x}$ (Lax-Wendroff method)

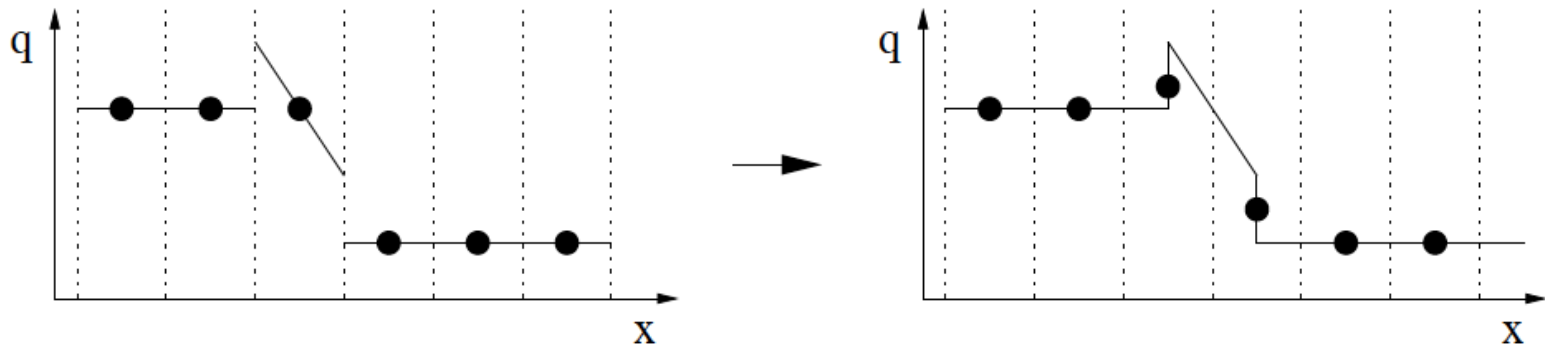
Higher-order now, but beware oscillations

„MUSCL (Monotonic Upwind-centered Scheme for Conservation Laws)“

Flux-conserving grid-based hydrodynamics

Piecewise linear subgrid model for flux:

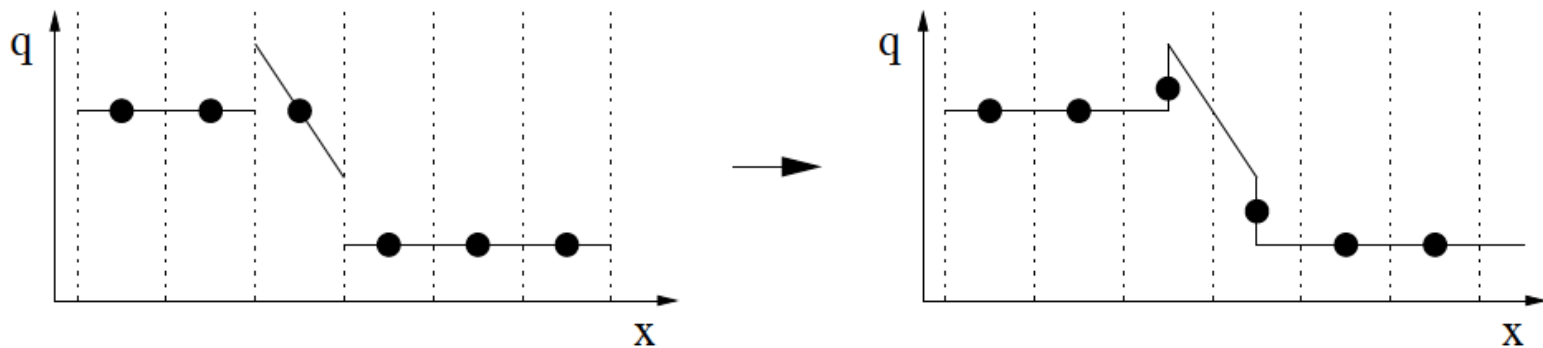
- can produce overshoots



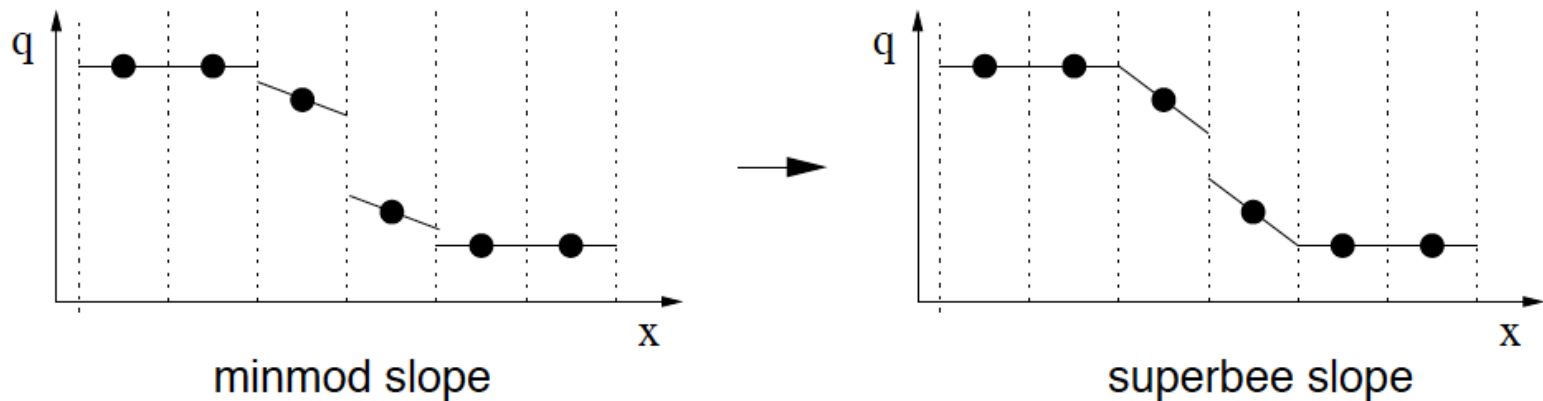
Flux-conserving grid-based hydrodynamics

Piecewise linear subgrid model for flux:

- can produce overshoots



Fix: slope limiters \rightarrow flux limiters



Flux-conserving grid-based hydrodynamics

Flux limiters:

- Normal flux:

$$f_{i+1/2}^{n+1/2} = \begin{cases} u_{i+1/2} q_i^n & \text{for } u_{i+1/2} > 0 \\ u_{i+1/2} q_{i+1}^n & \text{for } u_{i+1/2} < 0 \end{cases}$$

- Flux correction due to limiter Φ_i

$$\frac{1}{2} |u_i| \left(1 - |u_i| \frac{\Delta t}{\Delta x} \right) (q_i - q_{i-1}) \Phi_i$$

Flux-conserving grid-based hydrodynamics

Flux limiters:

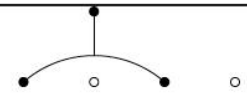
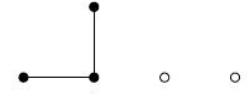
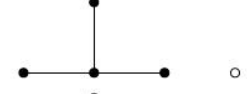
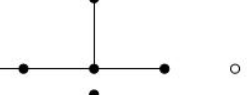
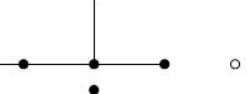

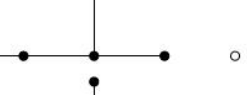


- Flux correction due to limiter Φ_i : $\frac{1}{2} |u_i| \left(1 - |u_i| \frac{\Delta t}{\Delta x} \right) (q_i - q_{i-1}) \Phi_i$

donor-cell :	$\phi(r) = 0$	$r_{i-1/2}^n = \begin{cases} \frac{q_{i-1}^n - q_{i-2}^n}{q_i^n - q_{i-1}^n} & \text{for } u_{i-1/2} \geq 0 \\ \frac{q_{i+1}^n - q_i^n}{q_i^n - q_{i-1}^n} & \text{for } u_{i-1/2} \leq 0 \end{cases}$	
Lax-Wendroff :	$\phi(r) = 1$		
Beam-Warming :	$\phi(r) = r$		
Fromm :	$\phi(r) = \frac{1}{2}(1 + r)$		linear
minmod :	$\phi(r) = \text{minmod}(1, r)$		non-linear
superbee :	$\phi(r) = \max(0, \min(1, 2r), \min(2, r))$		
MC :	$\phi(r) = \max(0, \min((1 + r)/2, 2, 2r))$		
van Leer :	$\phi(r) = (r + r)/(1 + r)$		

Flux-conserving grid-based hydrodynamics

Flux limiters:

- Flux correction due to limiter $\Phi_i : \frac{1}{2} |u_i| \left(1 - |u_i| \frac{\Delta t}{\Delta x} \right) (q_i - q_{i-1}) \Phi_i$

Name	Order	Lin?	Stable?	TVD?	Stencil
Two-point symmetric	1	lin	-	-	
Upwind / Donor-cell	1	lin	+	+	
Lax-Wendroff	2	lin	+	-	
Beam-warming	2	lin	+	-	
Fromm	2	lin	+	-	
Minmod	2/1	non-lin	+	+	
Superbee	2/1	non-lin	+	+	
MC	2/1	non-lin	+	+	
van Leer	2/1	non-lin	+	+	

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construction of classic 1D hydro solver

$$\begin{aligned}\partial_t \rho + \nabla \cdot (\rho \vec{u}) &= 0 \\ \partial_t(\rho \vec{u}) + \nabla \cdot (\rho \vec{u} \vec{u}) &= -\nabla P \\ \partial_t(\rho e_{\text{tot}}) + \nabla \cdot (\rho e_{\text{tot}} \vec{u}) &= -\nabla \cdot (P \vec{u})\end{aligned}$$

Source terms

HYDRO STEP:

1. Use standard advection scheme to advect ρ , $\rho \vec{u}$, ρe_{tot} with zero source
2. Treat source terms separately ([operator splitting](#))

Advantage of operator splitting: source terms cancel exactly (not inside the advection)

Code for hydro step; test with interacting sound waves

The basics of grid-based hydrodynamics

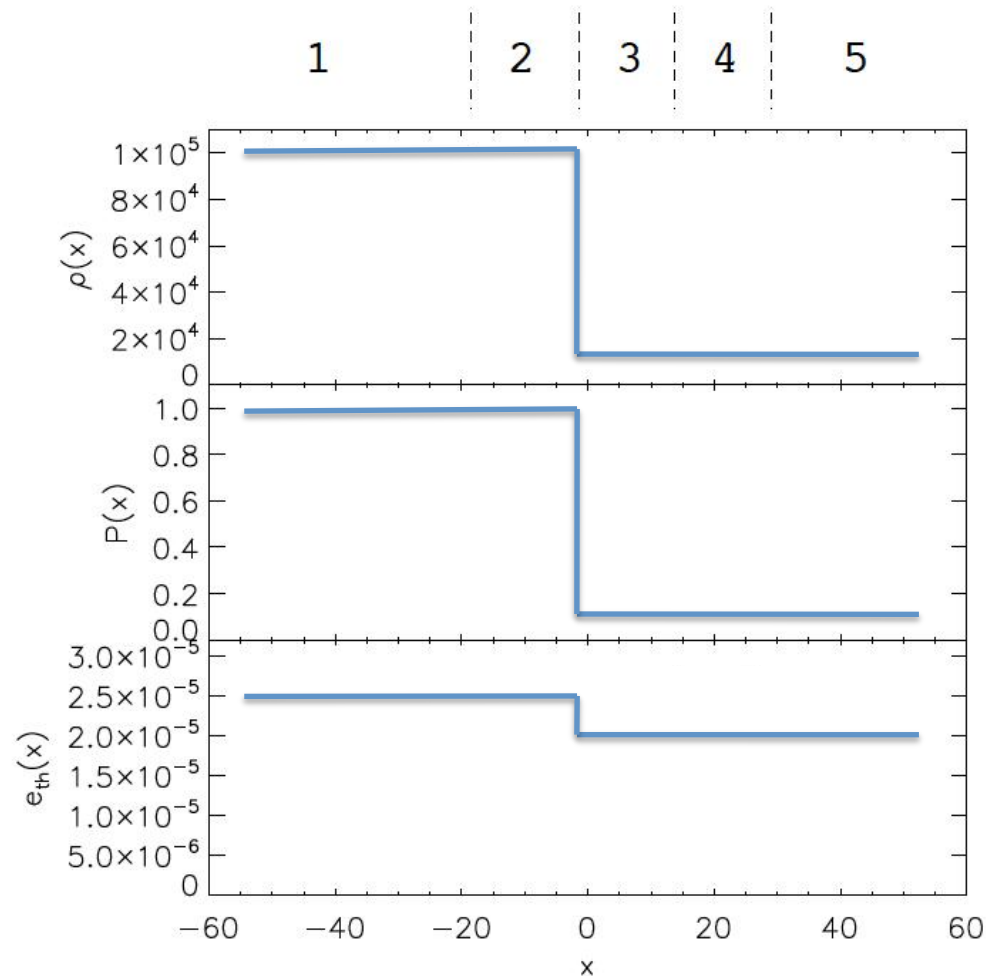
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Treating shocks – Riemann solvers

- Code treats smooth flows fairly well
- But shocks are common in astrophysics (e.g., interstellar medium)
- Flow speed is supersonic, i.e., $u > c_s$
- Need to solve Riemann problem
- Leads to Riemann solvers (e.g., Piecewise Parabolic Method)
Collela & Woodward (1984)

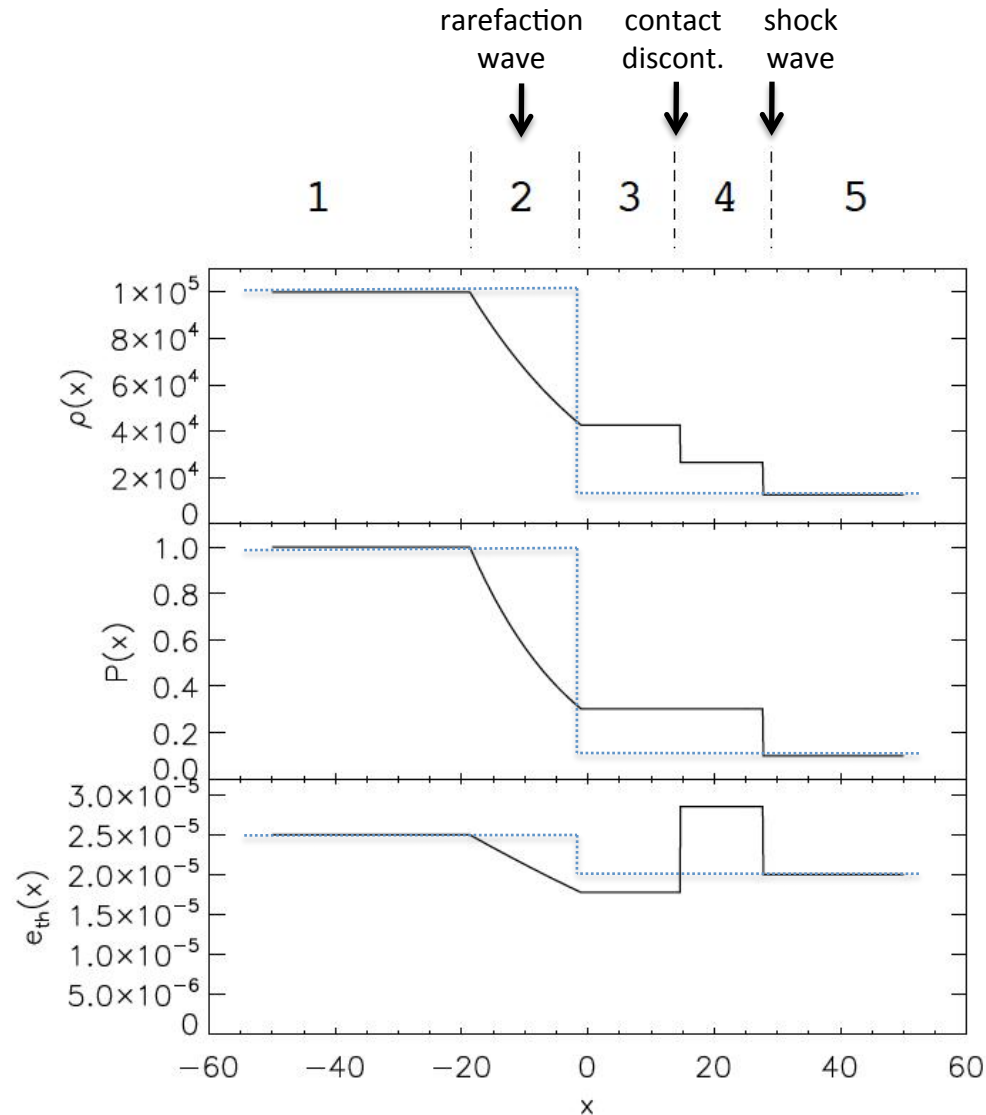
Difference to previous solver:
pressure terms are included in the advection

Sod shocktube test: $\rho_l = 10^5, P_l = 1$ $\rho_r = 1.25 \times 10^4$ and $P_r = 0.1$
 (Sod 1978)



Treating shocks

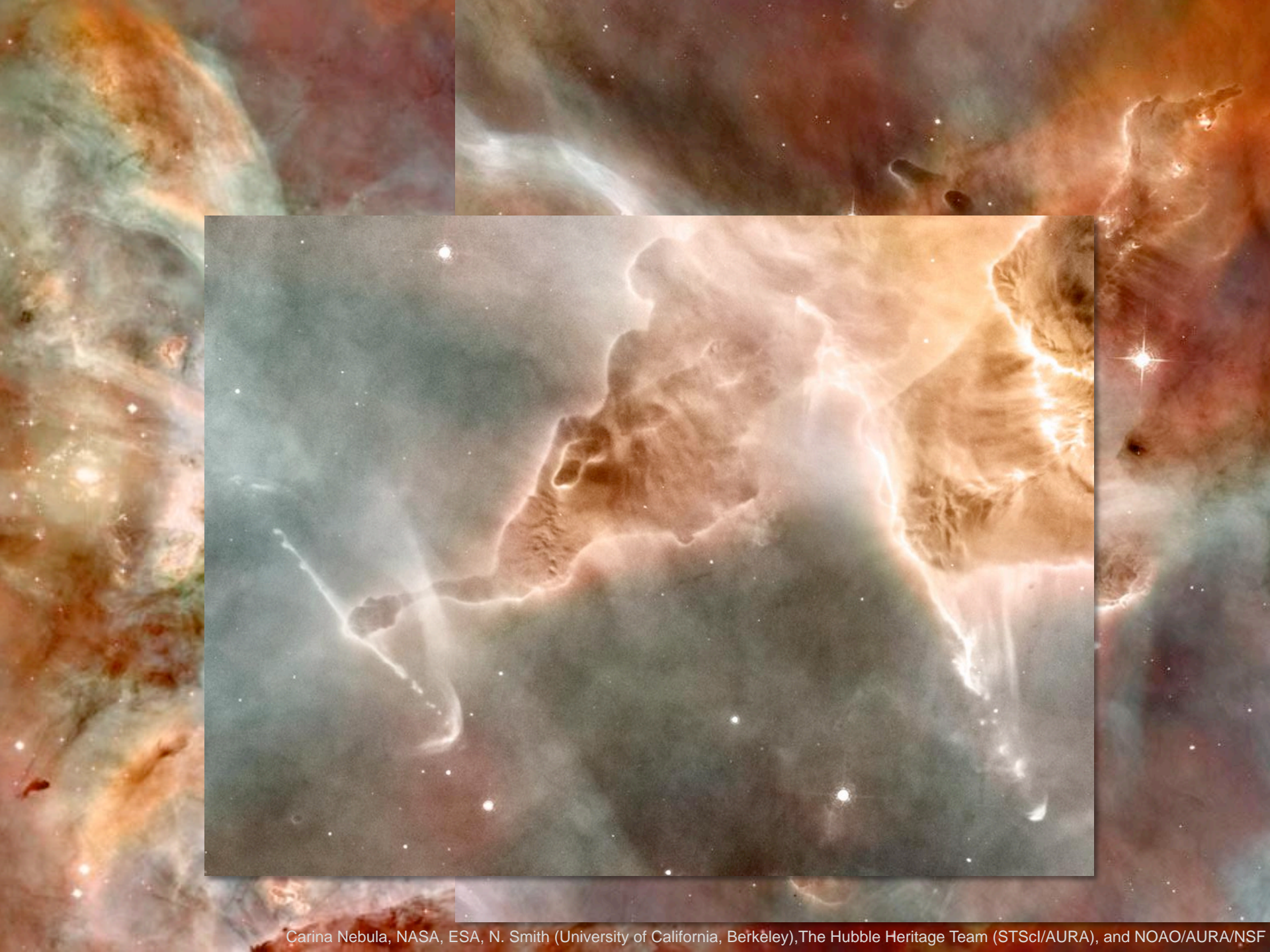
Sod shocktube test: $\rho_l = 10^5, P_l = 1$ $\rho_r = 1.25 \times 10^4$ and $P_r = 0.1$
(Sod 1978)



Sod shocktube test in 1D and 2D with AMR

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- Quantify fragmentation and accretion
- Prevent code from stalling

$$t_{\text{ff}} = \left(\frac{3\pi}{32G\rho} \right)^{1/2}$$

- Quantify fragmentation and accretion
- Prevent code from stalling

$$t_{\text{ff}} = \left(\frac{3\pi}{32G\rho} \right)^{1/2}$$

- Resolve fragmentation scale

$$\lambda_{\text{J}} = \left(\frac{\pi c_s^2}{G\rho} \right)^{1/2}$$

$$M_{\text{J}}(\rho) = \frac{4\pi}{3} \left(\frac{\lambda_{\text{J}}(\rho)}{2} \right)^3 \rho$$

Truelove et al. (1997)

Bate & Burkert (1997)

- Quantify fragmentation and accretion
- Prevent code from stalling

$$t_{\text{ff}} = \left(\frac{c}{32G\rho} \right)^{1/2}$$

- Resolve fragmentation

Cut off runaway collapse

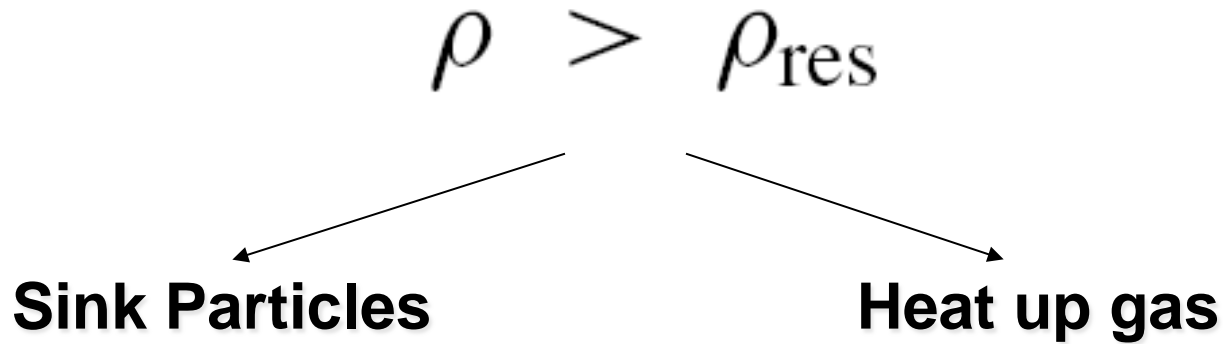
$$\lambda_{\text{J}} = \left(\frac{s}{G\rho} \right)^{1/2}$$

$$M_{\text{J}}(\rho) = \frac{4\pi}{3} \left(\frac{\lambda_{\text{J}}(\rho)}{2} \right)^3 \rho$$

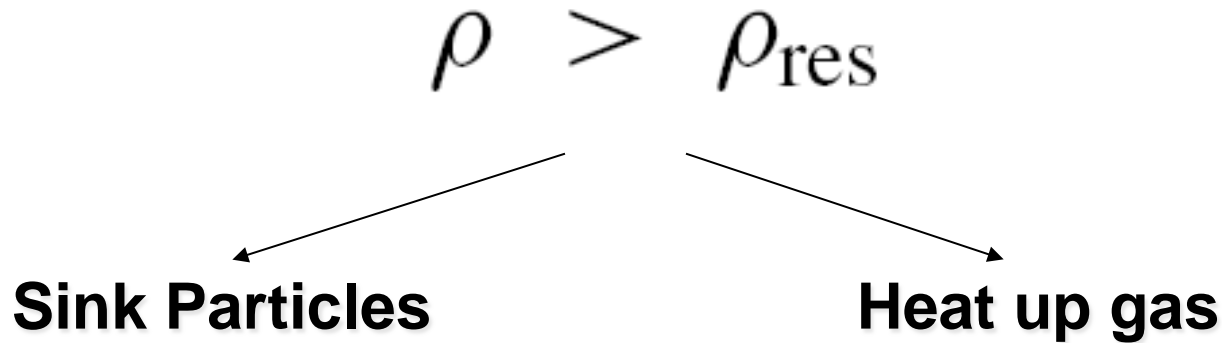
Truelove et al. (1997)

Bate & Burkert (1997)

Cut off runaway collapse



Cut off runaway collapse



1. Problem:

Courant time step

$$\min_{i,j,k} \left(\frac{\Delta x}{\max(|\mathbf{v}(i, j, k)|, c_s)} \right)$$

2. Problem:

changes EOS,

unless

$$\rho_{\text{res}} > 10^{-14} \text{ g cm}^{-3}$$

Cut off runaway collapse

$$\rho > \rho_{\text{res}}$$

Sink Particles

Heat up gas

Problem:

Spurious sink creation in shocks that DON'T go into free fall collapse

e.g., isothermal shock:
(Density~Mach²)

1. Problem:

Courant time step

$$\min_{i,j,k} \left(\frac{\Delta x}{\max(|\mathbf{v}(i, j, k)|, c_s)} \right)$$

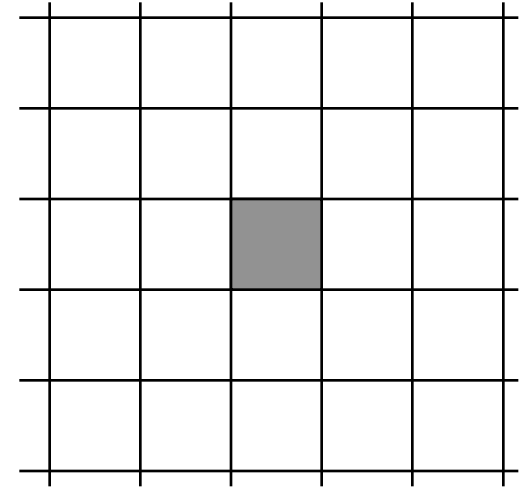
2. Problem:

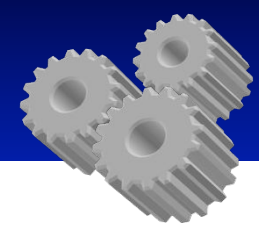
changes EOS,
unless

$$\rho_{\text{res}} > 10^{-14} \text{ g cm}^{-3}$$

Collapse checks to avoid spurious sink creation

1. Cell exceeds density threshold, $\rho > \rho_{\text{res}}$

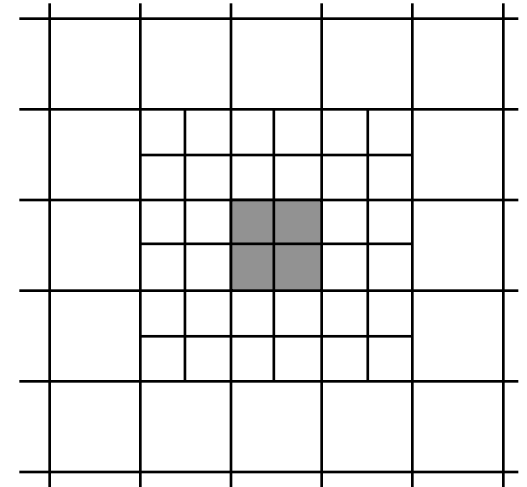




Sink particle implementation in FLASH

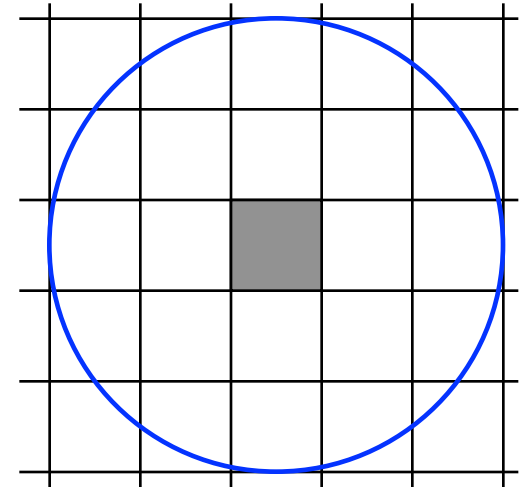
Collapse checks to avoid spurious sink creation

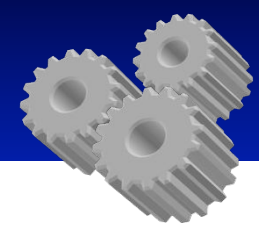
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Collapse checks to avoid spurious sink creation

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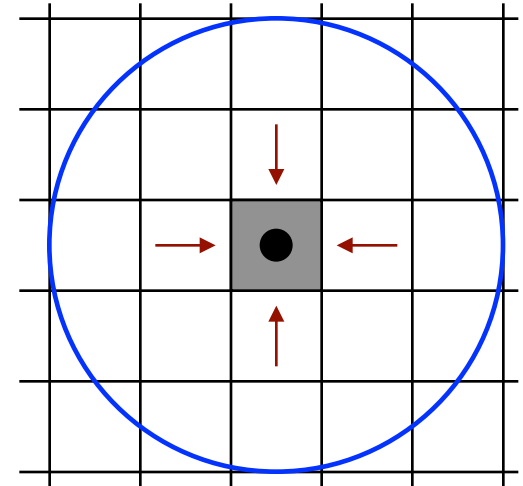


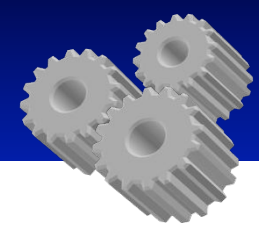


Sink particle implementation in FLASH

Collapse checks to avoid spurious sink creation

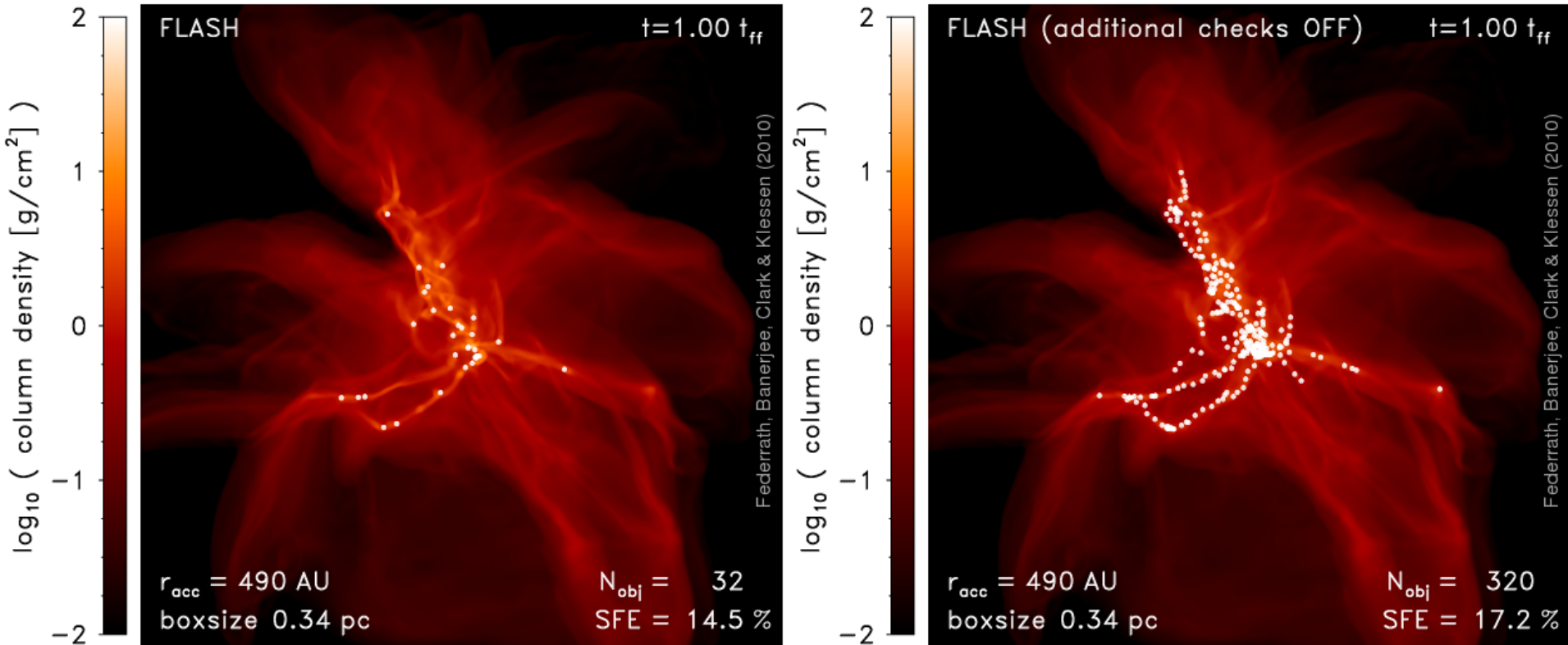
1. Cell exceeds density threshold, $\rho > \rho_{\text{res}}$
2. Highest level of AMR
3. Converging toward the center
4. Central minimum in gravitational potential
5. Jeans unstable, $|E_{\text{grav}}| > 2E_{\text{th}}$
6. Bound, $E_{\text{grav}} + E_{\text{th}} + E_{\text{kin}} + E_{\text{mag}} < 0$
7. Not within the accretion radius of an existing sink particle





Sink particle implementation in FLASH

Movies available: <http://www.mso.anu.edu.au/~chfeder/pubs/sinks/sinks.html>



all checks ON

$\rho > \rho_{res}$
only

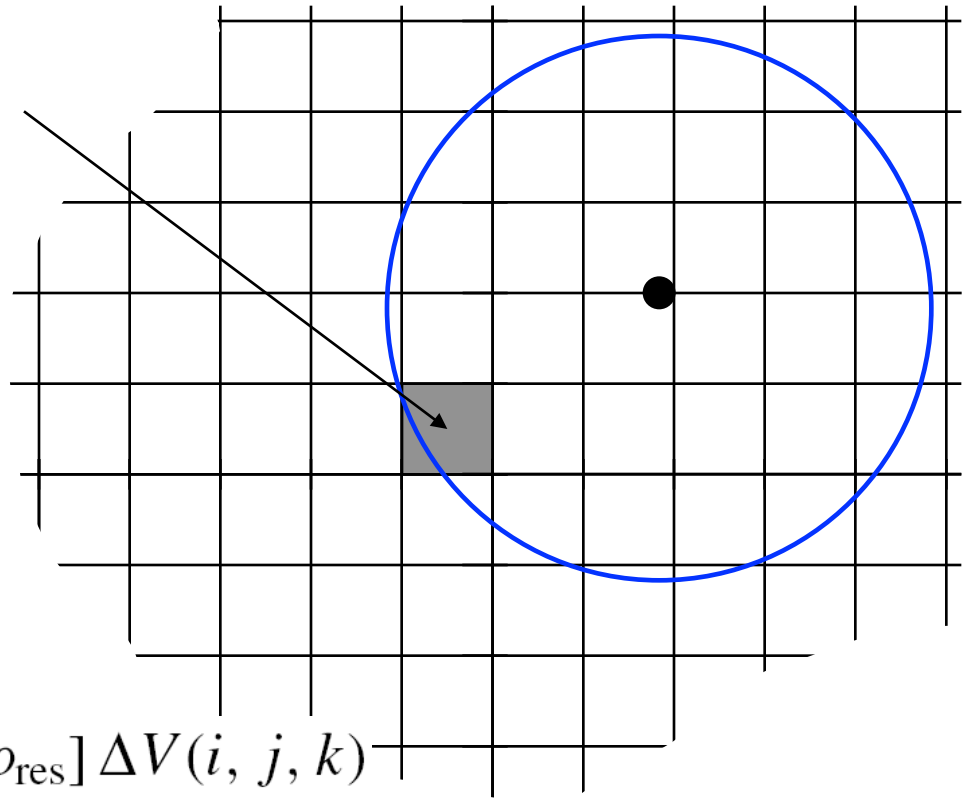
Federrath, Banerjee, Clark, Klessen (2010, ApJ 713, 269)

Sink particle implementation in FLASH

Gas accretion

$$\rho > \rho_{\text{res}}$$

1. Gas must be bound to the sink
2. Gas must be moving towards the sink



$$\Delta M = [\rho(i, j, k) - \rho_{\text{res}}] \Delta V(i, j, k)$$

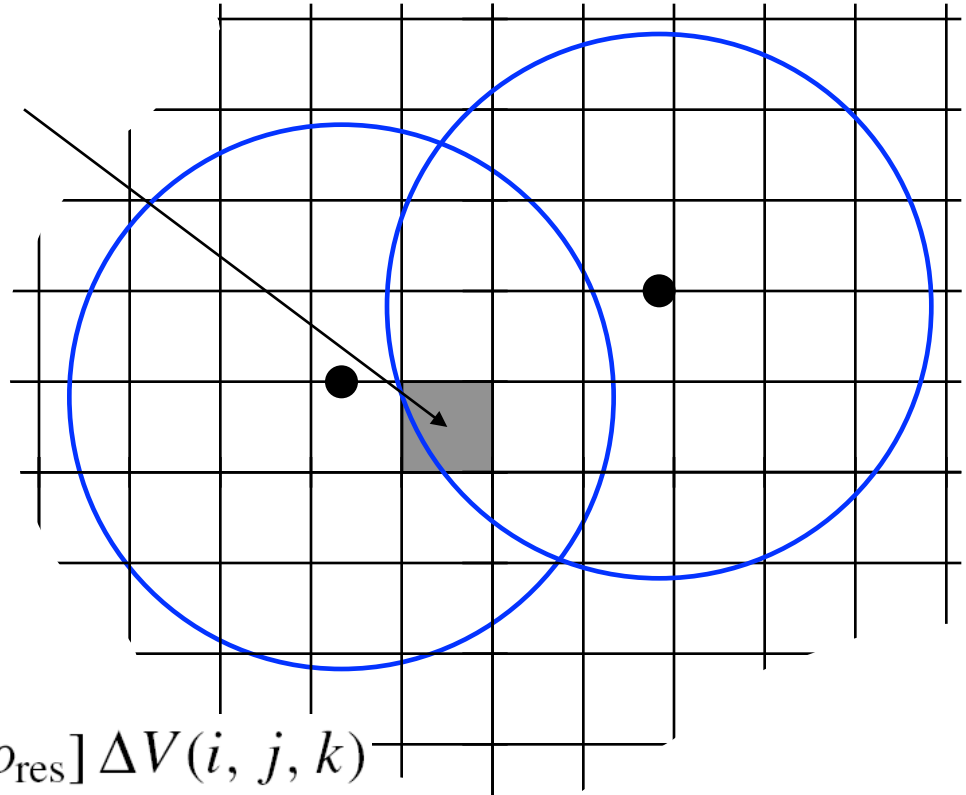
Mass, momentum, angular momentum conservation

Sink particle implementation in FLASH

Gas accretion

$$\rho > \rho_{\text{res}}$$

1. Gas must be bound to the sink
2. Gas must be moving towards the sink



Mass, momentum, angular momentum conservation

Gravitational interactions

Gas—Gas (multigrid solver, tree solver)

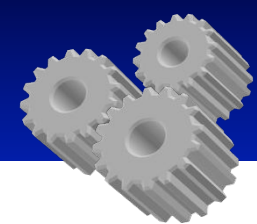
Gas—Sinks (interpolation from grid)

Sinks—Gas (direct summation, all cells)

Sinks—Sinks (direct N-Body summation)

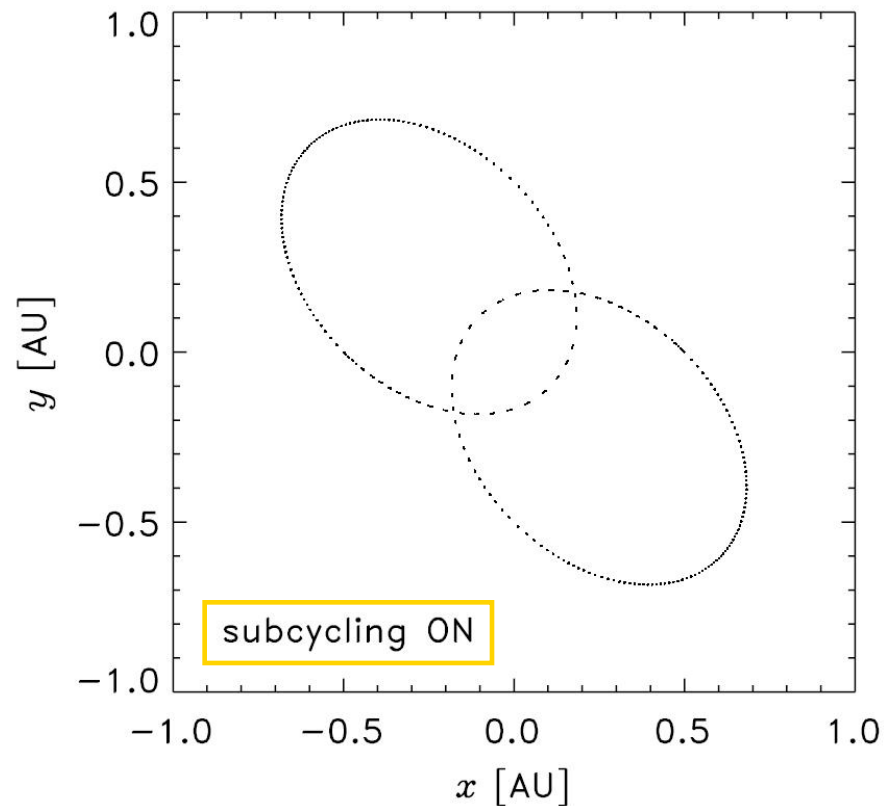
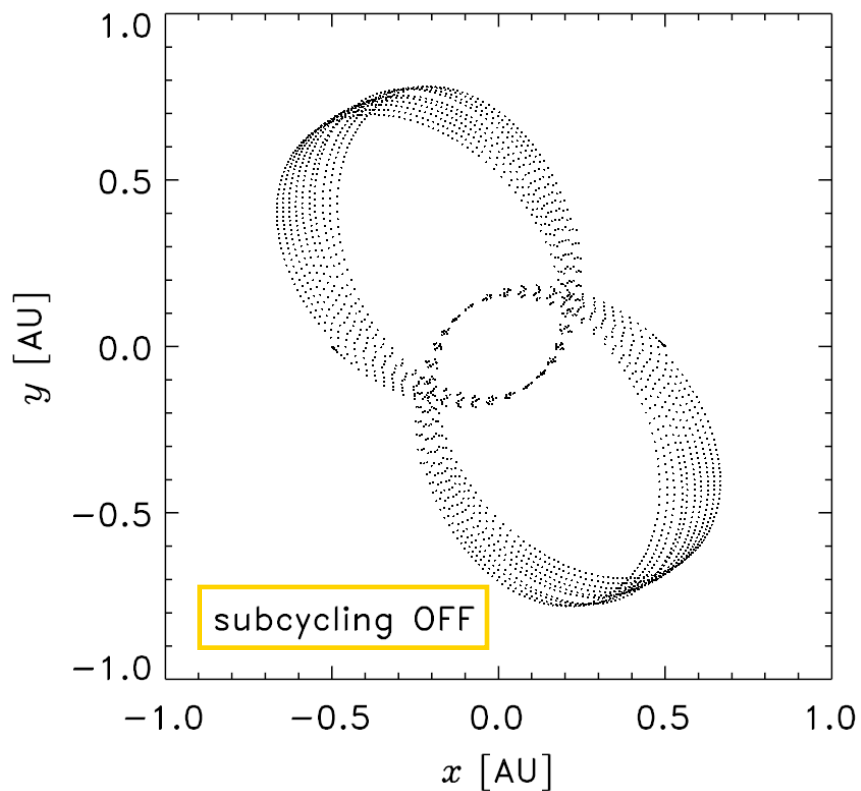
↙
Strong constraints on timestep

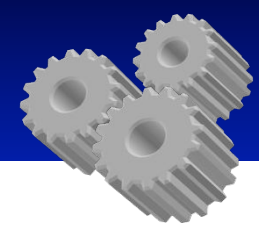
→ Subcycling with Leapfrog required



Sink particle implementation in FLASH

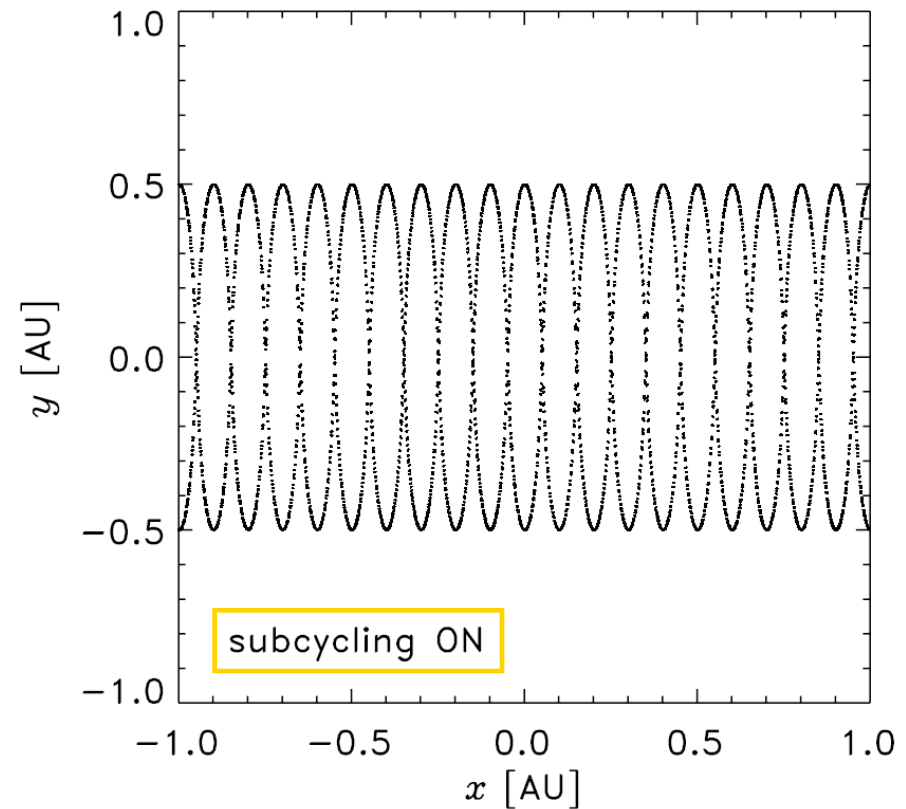
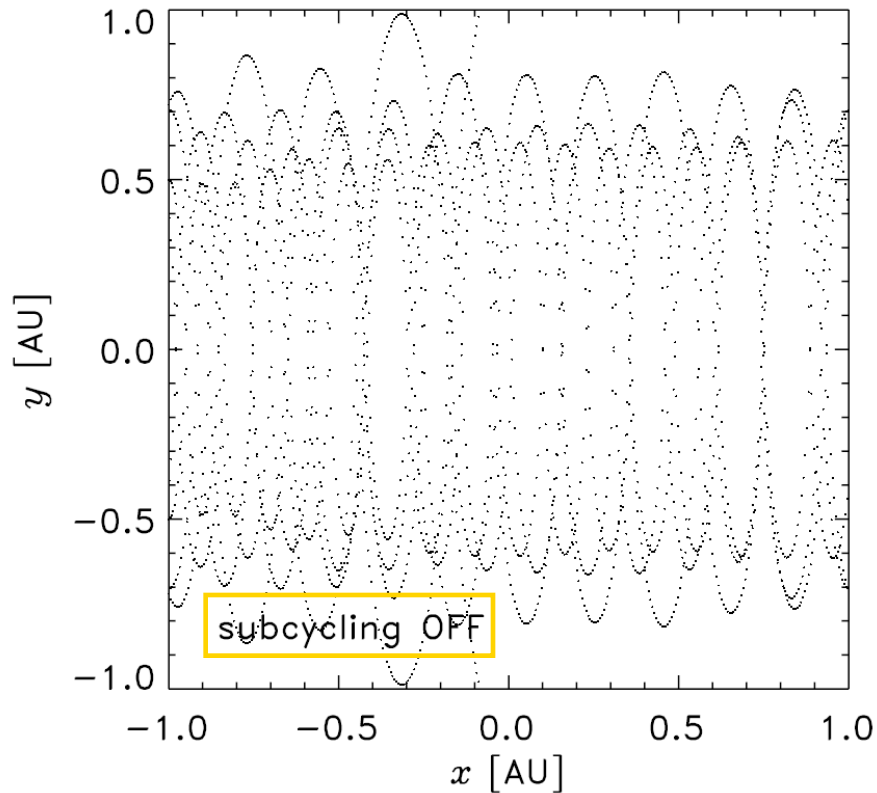
Subcycling required to capture N-Body dynamics



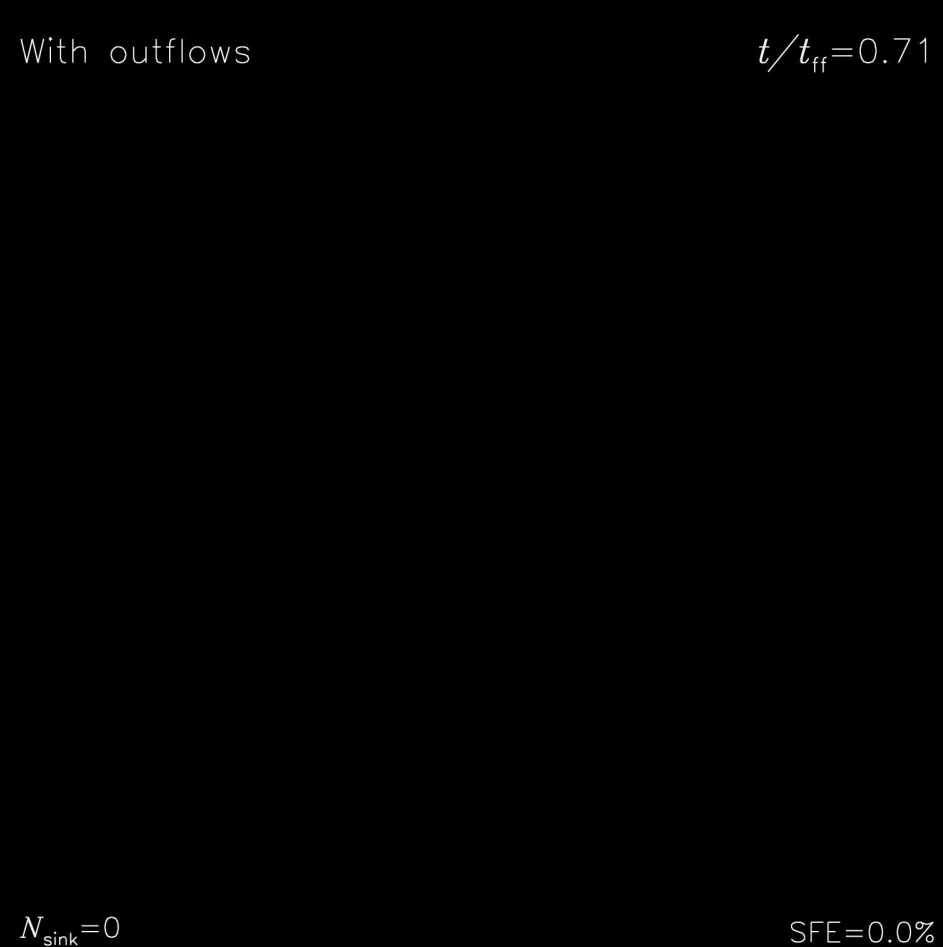
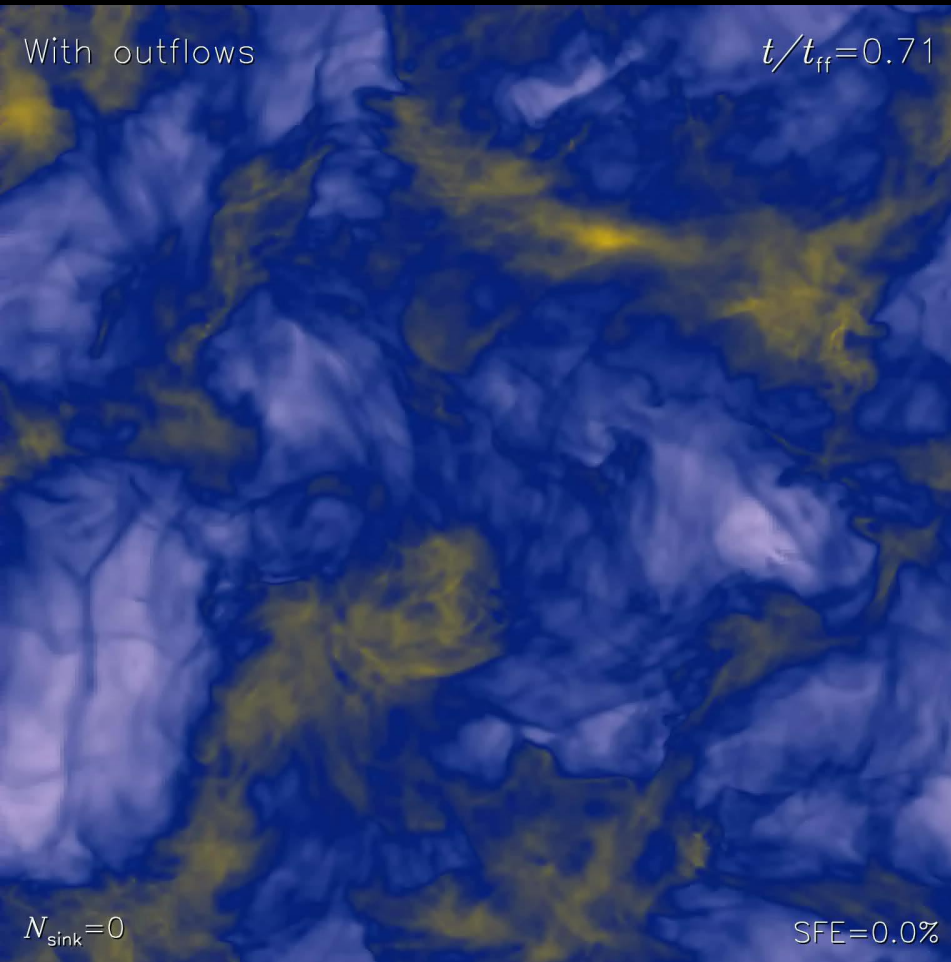


Sink particle implementation in FLASH

Subcycling required to capture N-Body dynamics



Grid-based Magnetohydrodynamics with Sink Particles

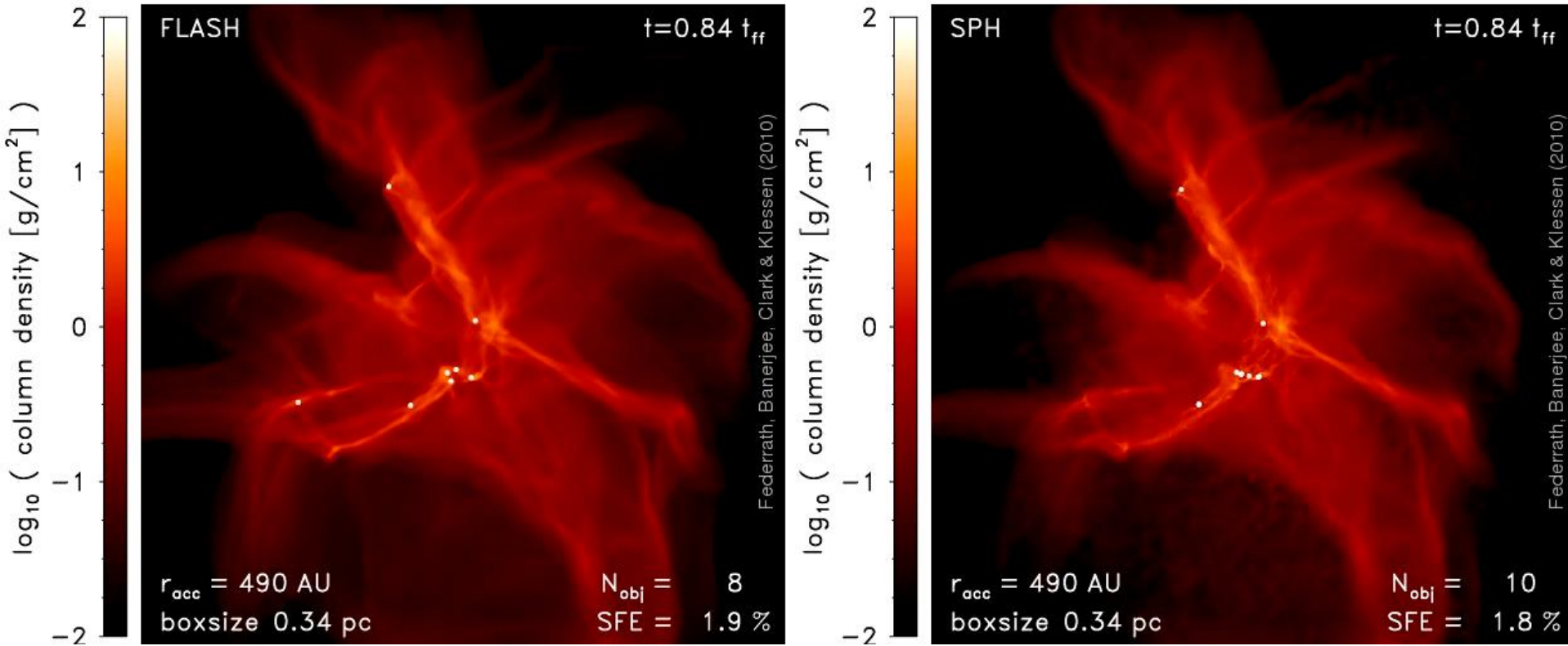


Movies available: http://www.mso.anu.edu.au/~chfeder/pubs/outflow_model/outflow_model.html

Sink particles: AMR versus SPH

Sink particles: AMR versus SPH

Movies available: <http://www.mso.anu.edu.au/~chfeder/pubs/sinks/sinks.html>



FLASH (AMR)

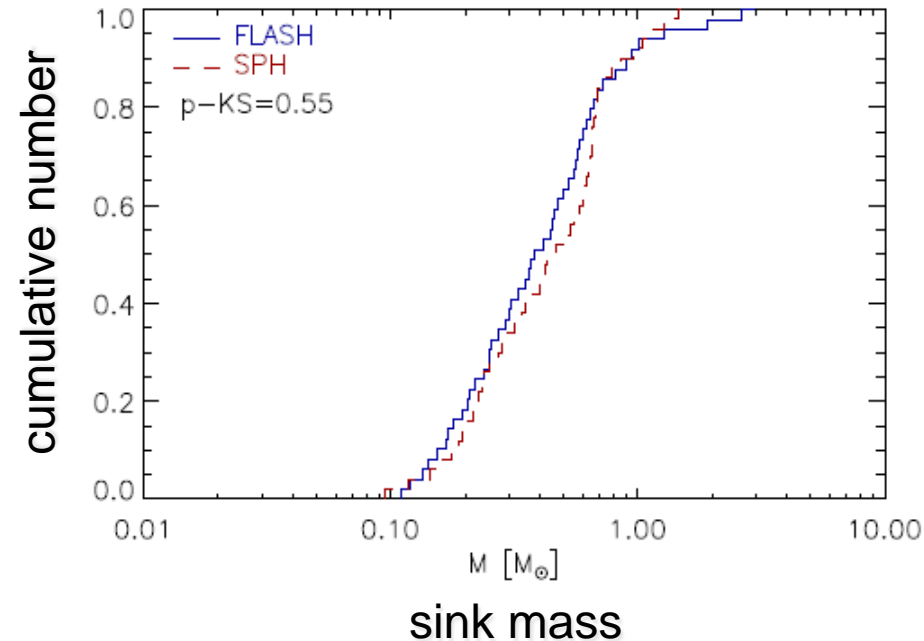
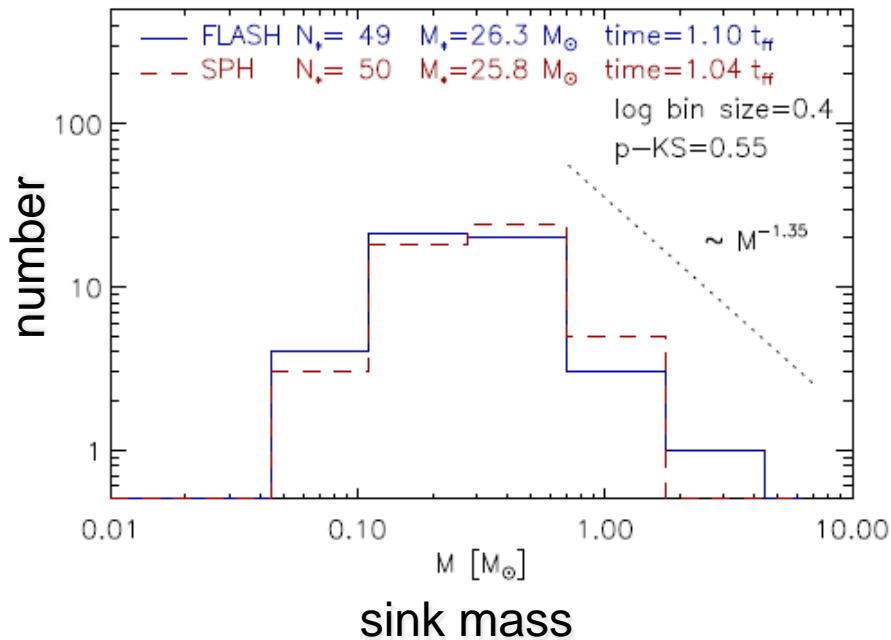
SPH

Federrath, Banerjee, Clark, Klessen (2010, ApJ 713, 269)

Sink particles: AMR versus SPH

Comparison for SFE $\sim 26\%$

1. Sink mass functions agree well
2. Number of sinks: FLASH 49, SPH 50



(Federrath, Banerjee, Clark, Klessen 2010, ApJ 713, 269)

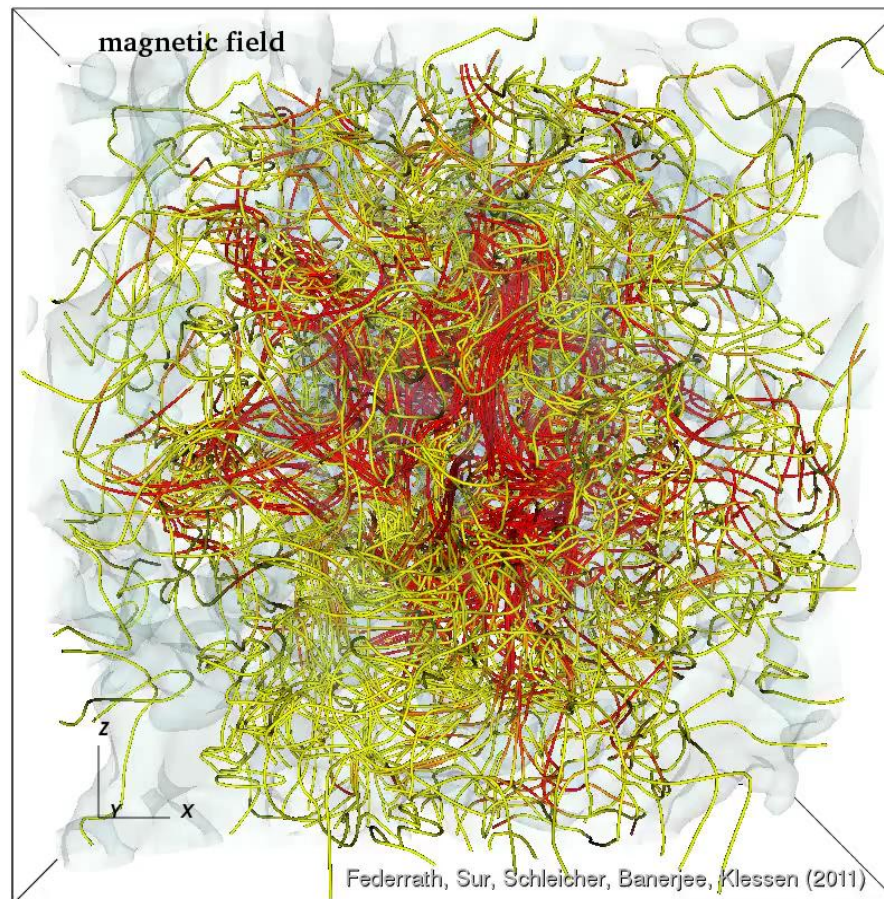
- **Sink creation checks** important to avoid spurious sinks in both SPH and AMR
 - **Encouraging agreement between FLASH and SPH-NG**
 - **computational cost:**
 - FLASH: 10,300 CPU hours, run on 128 CPUs
 - SPH-NG: 2,400 CPU hours, run on 16 CPUs
 - (AMR: factor of 30 more resolution elements necessary in FLASH)
- **SPH is faster in collapse calculations**
- ...but what about magnetic fields?

Magnetic fields in SPH and grid

- Problems with magnetic fields in SPH (Price & Federrath 2010)
- Divergence cleaning in SPMHD (Tricco & Price 2012)

http://www.mso.anu.edu.au/~chfeder/pubs/dynamo_grav/dynamo_grav.html

(Federrath, Sur, Schleicher, Banerjee, Klessen 2011, ApJ 731, 62)



Dynamo action

Strength and Weaknesses of SPH and grid

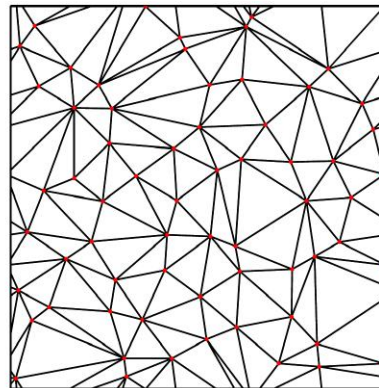
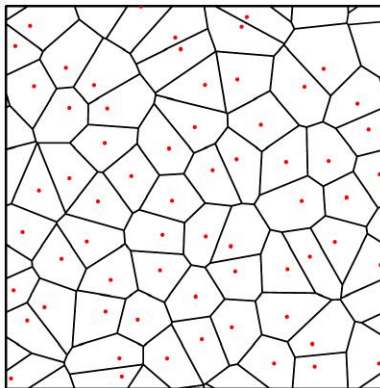
SPH

- + Automatic refinement on density
- + Typically faster in collapse calculations
- + More robust
- + Intrinsic mass conservation
- More complex data structure
- Problems with magnetic fields

Grid (AMR)

- + Simpler data structure (indexing)
- + Typically faster for pure hydro
- + Refinement on arbitrary quantities (e.g., position, shocks, etc.)
- + Magnetic fields
- Needs more resolution elements for collapse calculations (AMR)
- Sometimes less robust (solver crashes)

Unstructured Grid (e.g. AREPO)



Springel 2010

